Some issues for aggregate models of production systems

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Aggregate Simulations

Semiconductor fab¹

Usual model: Faithful representation of the factory using *Discrete Event Simulations*, e.g. χ (TU Eindhoven)

Problem:

Simulation of production flows with stochastic demand and stochastic production processes requires Monte Carlo Simulations

Takes too long for a decision tool

¹Dieter Armbruster, Daniel Marthaler, Christian Ringhofer, Karl Kempf,
Tae- Chang Jo: Operations Research **54**(5), 933 -950, 2006 → ★★★★★★★★★★★★★★★

A fluid model for a semiconductor fab

Fundamental Idea:

Model high volume, many stages, production via a fluid.

Basic variable

product density (mass density) $\rho(\mathbf{x}, \mathbf{t})$.

x- is the position in the production process, $x \in [0, 1]$.

- degree of completion
- stage of production

Mass conservation and state equations

Mass conservation and state equation

$$\frac{\partial \rho}{\partial t} + \frac{\partial F}{\partial x} = 0$$

$$F = \rho v_{eq}$$

Typical models for the equilibrium velocity v_{eq} (state equation) are

$$v_{eq}^{traffic}(
ho) = v_0(1 - rac{
ho}{
ho_c})$$
 $v_{eq}^Q = rac{\mu}{1+L}$
 $v_{eq} = \Phi(L)$

with L the total load (WIP) given as $L(\rho) = \int_0^1 \rho(x,t) dx$ Note: $\Phi(L)$ may be determined experimentally or theoretically



Equivalence

A clearing function $\Omega(L)$ giving the outflux as a function of WIP in steady state is completely equivalent to v_{eq} .

$$\Omega(L) = L v_{eq}$$

e.g.

$$\Omega_Q = \frac{\mu L}{1 + L}$$

$$\Omega_K = \alpha L (1 - e^{-\beta L})$$

Validation: DES vs. fluid simulation

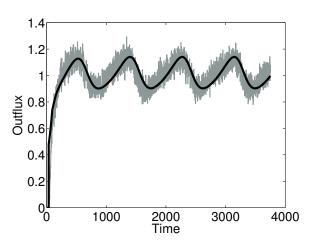


Figure: Throughput as a function of time for a sinusoidally varying input

Control of aggregate models

Control on the large scales

Tracking for a continuum model

Model: PDE model based on a product density $\rho(x,t)$ and a state equation for the velocity.

$$\rho_{t}(x,t) + v_{eq}^{Q} \rho_{x}(x,t) = 0, \quad (x,t) \in [0,1] \times [0,\infty)
\rho(x,0) = \rho_{0}(x), \quad x \in [0,1]
v_{eq}^{Q} = \frac{v_{max}}{1+L}
\lambda(t) = v(\rho)\rho(x,t)|_{x=0}$$

where $\lambda(t)$ is the influx.

Problem setup

- a fixed end time $\tau > 0$.
- an initial profile $\rho_0(x)$.
- d(t) the demand at time t. $d(t) \in L^2([0,\tau])$.

Find the influx $\lambda(t), t \in [0, \tau]$:s.t.

$$j(\rho,\lambda) = \frac{1}{2} \int_0^{\tau} \left(v_{eq}^Q(\rho) \rho(1,t) - d(t) \right)^2 dt$$

is minimal

Constraint Optimization

Method

- variational approach via adjoint calculus
- leads to two coupled PDEs
- solving allows to determine $\frac{dj(\lambda)}{d\lambda}$
- · gradient search algorithm finds a local minimum

System Reactivity

The speed

$$v = \frac{v_{max}}{1 + \int_0^1 \rho(s, t) \, ds}$$

depends on v_{max} .

Sinusoidal demands with:

- $v_{max} = 1$, inert factory
- $v_{max} = 3$, agile factory

Low Speed

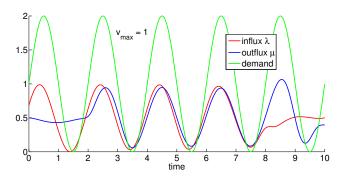


Figure: v_{max} of 1

High Speed

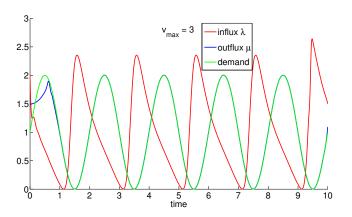


Figure: v_{max} of 3

Transient Clearing Functions²



Modeling transient behavior through clearing functions

Recall H. Missbauer's talk

- Consider an M/M/1 queue for a fixed time interval $[t, t + \tau]$ and an arrival rate $\lambda(t)$.
- Clearing function:

Expected output(
$$t$$
) = Φ (Expected load L)(t)

with

$$L(t) = w + A = w + \int_{t}^{t+\tau} \lambda(s) ds$$

w is the initial WIP.

• Result: Φ depends on w, the arrival A and variance of the initial WIP σ_w^2 .

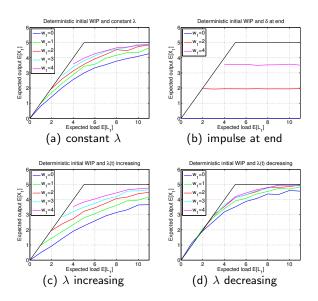
It is more complicated

Functional form of λ

Choose initial WIP, arrival A and vary $\lambda(t)$

- Choose $\lambda(t) = c$
- linearly increasing inter arrival rate
- linearly decreasing inter arrival rate
- impulse at s = 0
- impulse at $s = \tau$

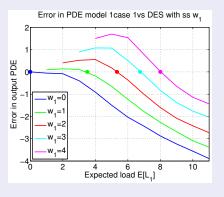
Results



How good is the PDE model for those transient cases?

PDE model is adiabatic

Should be good for slow changing influx.



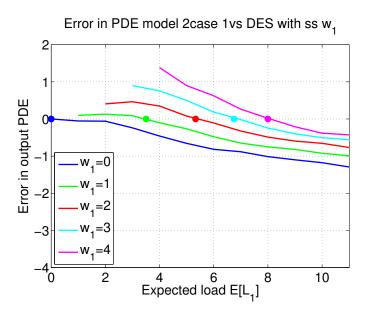
Modeling the time evolution of the velocity

$$\frac{\partial \rho}{\partial t} + \frac{\partial v \rho}{\partial x} = 0$$

$$\frac{\partial v}{\partial t} + v \frac{\partial v}{\partial x} = 0$$

$$\rho v|_{x=0}(t) = \lambda(t)$$

$$v(0,t) = v_{eq}(t)$$



Continuous models for production lines with finite buffers

Production lines with finite buffers

Current assumption

Buffers can become infinite ρ can have δ -measures flux may be restricted but not density

Production lines for larger items, e.g. cars

There exists only a small buffer between machines Need to implement a limit on ρ in our model

Experiment

100 identical machines with capacity $\mu=1$ all buffers between machines have identical capacity of $\it M$

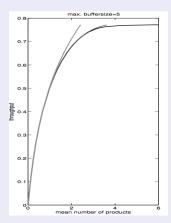
- f 1 fill an empty factory with a constant influx rate $\lambda < 1$
- 2 shut down the last machine
- 3 factory fills up and stops working when the first buffer is at its maximum.
- 4 restart last machine and drain the factory until it reaches steady state again.

 $^{^3}$ P. Goossens, Modeling of manufacturing systems with finite buffer sizes using PDEs, Masters Thesis, TU Eindhoven, 2007 $^{\circ}$ $^{\circ$

Phenomenology I

Model needs to explain:

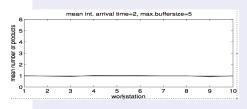
• The maximal steady state throughput λ_{max} of the production line is much lower than 1

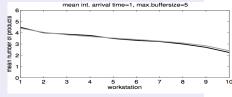


Phenomenology II

More:

- The steady–state WIP distribution $ho_{ss}(x)$ for $\lambda << 1$ is constant in x
- The steady–state WIP distribution $\rho_{ss}(x)$ for $\lambda \approx \lambda_{max}$ decays almost linearly in x





More:

 At shut down, the production line is filled up by a backwards moving wave.
 wave speed is

$$v_{shutdown} = \frac{\lambda}{M - \int_0^1 \rho_{ss}(x) dx}.$$
 (1)

- The transient drain depends on the influx λ .
 - If $\lambda \approx \lambda_{\it max}$ then the factory drains from the end.
 - If $\lambda < \lambda_{max}$ then WIP is reduced by a wave "eating" into it from upstream and at the same time WIP uniformly drains downstream.

Phenomenology IV

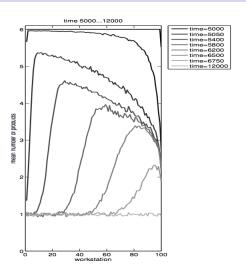


Figure: $\lambda < \lambda_{max}$. The WIP distribution drifts downwards and "gets eaten" from the back

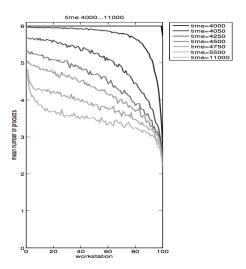


Figure: $\lambda \approx \lambda_{max}$, the system approaches the steady state distribution almost uniformly in space.

Inhomogeneous processing rate

Two fundamental stochastic processes

- The production process with mean processing rate $\mu = 1$.
- The blocking process when the buffer becomes full.

Together they lead to an inhomogeneous processing rate

$$\tilde{\mu} = c(x)\mu$$
.

We make three assumptions for c(x);

- c(1) = 1.
- c(x) linearly increases with the steady state influx λ .
- c(x) linearly increases as a function of x.

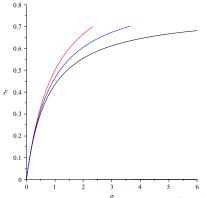
Consistent Assumption:

$$\tilde{\mu} = c(x)\mu = \lambda k(x-1) + \mu$$



Inhomogeneous and discontinuous flux

$$F(\rho, x) := \begin{cases} \frac{\mu \rho}{1 + \rho + k\rho(1 - x)} & \text{for } \rho < M \\ 0 & \text{for } \rho \ge M. \end{cases}$$
 (2)



Steady state WIP distribution

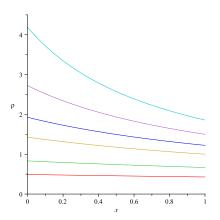


Figure: Steady states for a flux function (2) and different values for the inflow densities λ

Riemann problem

For different initial conditions we get different kinetic waves:

- a rarefaction speed $\lambda = f'(\rho)$. Filling wave start at a traffic light.
- a shock wave speed $s = \frac{f(\rho_l)}{\rho_l M}$. Blocking wave.
- a shock wave traveling with infinite speed. Information wave after restart.
- This wave is followed by a classical rarefaction wave emanating at x=1 and a shock wave emanating at x=0

First PDE Simulations I

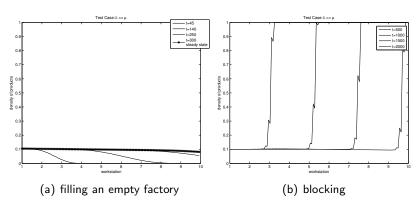


Figure: $\lambda < \lambda_{max}$.

First PDE Simulations II

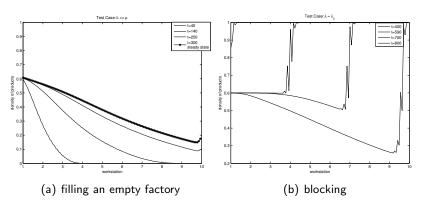


Figure: $\lambda \approx \lambda_{max}$.