# Cumulative Sum Control Charts for Covariance Matrix

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### Abstract

Cumulative sum (CUSUM) charts for controlling the covariance matrix are proposed via the projection pursuit method. Unlike traditional charts for covariance, the proposed charts can be used in a low-volume or short-run environment. It is shown that the proposed procedures are more effective than various existing ones. Their applications to monitoring a process with paired measurements are demonstrated. The CUSUM chart based on the likelihood ratio is also investigated. The performances of two new kinds of CUSUM charts are similar. However, the likelihood ratio based CUSUM chart requires that the size of each subgroup is larger than the dimension of the quality characteristics.

Keywords: Covariance Matrix, CUSUM Chart, Multivariable Control Chart, Projection Pursuit, Shewhart Type Control Chart.

A Short Running Title: CUSUM for Covariance Matrix

#### 1. Introduction

There are many situations in which the overall quality of a product is determined by several correlated quality characteristics. Alt(1985) effectively illustrated the need for multivariate control charts in such situations. Mason et al. (1997) discussed the implementation and interpretation issues. Various types of multivariate charts for process mean have been suggested (see, for example, Alt 1985, 1988; Jackson 1991; Lowry et al. 1992; Lowry and Montgomery 1995; Chan and Li 1994; Ngai and Zhang 1994; Flury et al. 1995; Wierda 1994) in the past decade. A brief introduction to the multivariate control problem can be found in Montgomery (1996, p322-330) and Ryan (1989, p215-227). Like the process mean, the process variability, usually summarized by a covariance matrix, is important for judging whether the process is in control. Two kinds of charts for covariance were suggested by Alt (1985). However, neither the problem of efficiently controlling the process

covariance nor the comparison of these charts have been well studied. We will study these in this paper.

The charts for covariance surveyed in Alt and Smith (1988) are of the Shewhart type, i.e., each plotted point is based only on an independent sample (also called subgroup). The Shewhart type chart is easy to implement. But they only use the information in an individual sample (i.e., subgroup). Such charts are insensitive to small or moderate changes of the covariance matrix. Another disadvantage is that these charts can be constructed only when each sample size is larger than the dimension of the quality characteristics. This is not always possible or practical. For example, as Ryan (1989, Chapter 6) points out, items coming off an assembly line may be produced at such a low rate that the process might have already gone out of control when a subgroup of sufficiently large size is formed. In the short-run environment, a large or moderate sample size is usually not feasible because of the low-volume manufacturing. A very extensive and comprehensive discussion on statistical process monitoring and control is given in a series of articles appearing in the April 1997 issue of Journal of Quality Technology (edited by D.C.Montgomery and W.H.Woodall).

To overcome these disadvantages, CUSUM type charts based on the projection pursuit technique (Huber 1985) are developed in this paper. In many cases the new charts can detect a change of covariance more than twice faster (i.e., half of the average run length) than some existing Shewhart charts. The CUSUM chart based on the likelihood ratio (LRC) is also investigated. Like the Shewhart charts, the condition that each sample size is larger than the dimension of the quality characteristics is required in constructing the LRC. Our study shows that the projection pursuit based CUSUM chart with the reference values 1.5 and 0.5 performs better than the LRC in detecting a upward change of covariance. However, the conclusion is reversed when a certain degree of downward changes are presented in the covariance. We also show that we can adjust the reference values so that the projection pursuit based CUSUM chart has performances similar to LRC in detecting both upward and downward changes.

The proposed charts can be used for quality control of a paired measurement system. In some situations, the precision of process measurements depends on product variability as well as measurement error. Paired measurements on each single specimen from two or more laboratories are made to account for these two sources of variation. Control charts for such a process have been investigated recently (for example, Jackson (1991); Tracy et al. (1995)). The new charts can simultaneously monitor both sources of variation.

#### 2. Principles of the New Charts

Consider a p-dimensional random vector X, which represents p quality characteristics and is normally distributed with mean  $\mu$  and covariance (matrix)  $\Sigma$ . A sample of size n ( $n \ge 1$ ) is taken from the process over each time period. The *i*-th sample is denoted by  $x_{ik}$ ,  $k = 1, \dots, n$ . The aim of a multivariate control chart is to detect the possible deviations of process mean and covariance

from the nominal values  $(\mu_0, \Sigma_0)$  which are assumed to be known in advance, while it gives as few "false alarms" as possible. In terms of the run length (RL) of the chart, a chart should ideally have a long RL when the process is in-control and a short RL when the process is out-of-control. The run length is defined as the number of samples to be taken before receiving an out-of-control signal. Here, we call the RL in-control RL or out-of-control RL depending on whether the process is actually in- or out-of-control.

# 2.1. PP Approach

The projection pursuit (PP) method is a powerful tool for developing this kind of multivariate chart for the mean (see, Huber, 1985; Ngai and Zhang 1994). The PP approach to control chart for covariance is based on the following Principles (see Appendix I for the proof):

- (i)  $\Sigma = \Sigma_0$  if and only if  $a_{max}^{\top} \Sigma_0^{-1/2} X$  and  $a_{min}^{\top} \Sigma_0^{-1/2} X$  have unit variance, where  $a_{max}$  and  $a_{min}$  are the eigenvectors correspond, respectively, to the largest and smallest eigenvalues of the matrix  $\Sigma_0^{-1/2} \Sigma \Sigma_0^{-1/2}$ , and  $\Sigma_0^{-1/2}$  denotes the inverse of the square root of  $\Sigma_0$  and  $a^{\top}$  is the transpose of a;
- (ii)  $a_{max}$  and  $a_{min}$  will give the maximum and the minimum (signed) differences between the variance of  $a^{\top} \Sigma_0^{-1/2} X$  and the unit value 1, respectively.

Principle (i) implies that in order to test whether the covariance matrix of X deviates from the nominal  $\Sigma_0$ , it suffices to make two univariate tests for the null hypotheses  $H_{max0}$ : "the variance of  $a_{max}^{\top} \Sigma_0^{-1/2} X$  is equal to 1" and  $H_{min0}$ : "the variance of  $a_{min}^{\top} \Sigma_0^{-1/2} X$  is equal to 1", respectively, via the projected and transformed samples  $a_{max}^{\top} \Sigma_0^{-1/2} x_{ik}$ , and  $a_{min}^{\top} \Sigma_0^{-1/2} x_{ik}$ , where  $1 \leq k \leq n$ ,  $i = 1, 2 \cdots$ . In practice  $a_{max}$  and  $a_{min}$  depend on  $\Sigma$ , and are unknown and have to be estimated. Let, for each  $a, T_i(a)$  be an univariate statistic for testing  $H_{max0}$ , such that the larger value of  $T_i(a)$  gives the stronger evidence against  $H_{max0}$ . Then Principle (ii) suggests if an estimator  $\hat{a}_{max}$  gives the maximum value of  $T_i(a)$ , it is a natural estimator of  $a_{max}$  in the i-th time period. Consequently,  $T_i(\hat{a}_{max})$  is a natural test statistic for  $H_{max0}$  in the i-th period. Similarly, we can define  $\hat{a}_{min}$  and test  $H_{min0}$  by  $T_i(\hat{a}_{min})$ .

In summary, PP approach contains two key steps: (1) selecting a univariate control chart for variance with a test statistic  $T_i$ ; (2) estimating  $a_{max}$  and  $a_{min}$  iteratively over each time period i and calculating the values of  $T_i(\hat{a}_{max})$  and  $T_i(\hat{a}_{min})$ .

There are several well developed univariate control charts for variance. The most well-known and relatively efficient ones are the CUSUM chart of Johnson and Leone (1962) and the exponentially weighted moving average (EWMA) chart by Chang and Gan (1995). We choose the Johnson-Leone CUSUM chart here (the PP extensions of the EWMA procedure is similar in principle). So the remaining step is to calculate  $\hat{a}_{max}$ ,  $\hat{a}_{min}$ ,  $T_i(\hat{a}_{max})$  and  $T_i(\hat{a}_{min})$  for the Johnson-Leone chart.

# Case 1: Using individual observations

The Johnson-Leone chart for variance is derived from the sequential test. Let  $x_i$  be the observation of a univariate process at the *i*-th time period. The nominal value  $\sigma_0 = 1$ . Assume the process

mean is zero and in-control. Let  $k_l < k_u$  be two reference values. For example, we frequently use values  $k_u = 1.5$  and  $k_l = 0.5$ . Set

$$SU_0 = 0$$
,  $SU_i = \max\{0, SU_{i-1} + x_i^2 - k_u\}$ ,  $SL_0 = 0$ ,  $SL_i = \min\{0, SL_{i-1} + x_i^2 - k_i\}$ ,  $i > 1$ 

 $SU_i$  and  $SL_i$  are called the *i*-th CUSUM values. The Johnson-Leone chart is defined to indicate an out-of-control message as soon as  $SU_i > h_u$  or  $SL_i < h_l$ , where  $h_u$  and  $h_l$  are the respective upper and lower control limits. For simplicity, we let  $h_u = h = -h_l > 0$ . However, it is possible to improve the performance of the CUSUM chart by choosing some non symmetric pair values of  $(h_l, h_u)$ .

Let  $x_i$  be the observation of a p-dimensional process at the i-th time period. For simplicity, we assume that the nominal values  $\mu_0 = 0$  and  $\Sigma_0 = I_p$  (p by p unit matrix). We also assume that the process mean is stable. In light of the above, to estimate  $a_{max}$  and  $a_{min}$ , we first define the CUSUM values for each direction a:

$$SU_0^a = 0, \quad SU_i^a = \max\{0, SU_{i-1}^a + (a^\top x_i)^2 - k_u\},$$
 
$$SL_0^a = 0, \quad SL_i^a = \min\{0, SL_{i-1}^a + (a^\top x_i)^2 - k_l\}, \quad i \ge 1.$$

According to Johnson and Leone (1962), when  $a^{\top}x_i$  is normally distributed,  $\{SU_i^a\}$  and  $\{SL_i^a\}$  are the likelihood ratio statistics for testing the hypotheses,  $H_{max0}$  and  $H_{min0}$ . Even if  $a^{\top}x_i$  is not normally distributed,  $SU_i^a$  and  $SL_i^a$  can be still used. This is because it can be shown that when i is large,  $T_i(a) = SU_i^a$  is approximately proportional to the difference between the variance of  $a^{\top}X$  and the nominal value 1 when the difference exceeds  $k_u - 1$  (see Appendix II); a similar conclusion holds for  $SL_i^a$  when the difference is less than  $k_l - 1$ . As already mentioned, it is natural to estimate  $a_{max}$  and  $a_{min}$  by  $a_{imax}$  and  $a_{imin}$  in which  $SU_i^a$  and  $SL_i^a$  attain the maximum and minimum, respectively.

To simplify the notion, we denote  $SU_i^{\hat{a}}$  and  $SL_i^{\hat{a}}$  by  $SU_i$  and  $SL_i$ , respectively. Let  $\lambda_{ij}^u$  and  $\lambda_{ij}^l$  be the largest and the smallest eigenvalues of the sample matrix  $x_i x_i^{\top} + \cdots + x_j x_j^{\top}$ ,  $1 \leq j \leq i$  respectively. Define

$$SU_{ij} = \lambda_{ij}^u - (i - j + 1)k_u, \quad SL_{ij} = \lambda_{ij}^l - (i - j + 1)k_l, \quad 1 \le j \le i.$$

Then it can be shown that

$$SU_{i} = \max_{\|a\|=1} SU_{i}^{a} = \max\{0, SU_{i1}, \dots, SU_{ii}\},$$

$$SL_{i} = \min_{\|a\|=1} SL_{i}^{a} = \min\{0, SL_{i1}, \dots, SL_{ii}\}.$$
(2.1)

And if u(i) and l(i) are such that  $SU_{iu(i)} = SU_i$  and  $SL_{il(i)} = SL_i$ , then  $\hat{a}_{imax}$  and  $\hat{a}_{imin}$  are the eigenvectors corresponding to the largest eigenvalue of  $x_i x_i^{\top} + \cdots + x_{u(i)} x_{u(i)}^{\top}$  and the smallest eigenvalue of  $x_i x_i^{\top} + \cdots + x_{l(i)} x_{l(i)}^{\top}$ , respectively.

Now the CUSUM chart for covariance, to be denoted by  $MCD_1(0)$ , where the subscript means sample size is 1 can be defined to indicate an out-of-control message when  $SU_i > h_u$  or  $SL_i < h_l$ .

The CUSUM values  $\{SU_i\}$  and  $\{SL_i\}$  can be separately used to detect a upward change (an inflation) and a downward change (a shrinkage) of covariance, that is, there is a direction in which the variance of the projected process increases or decreases.

A simulation study indicates that  $MCD_1(0)$  is sensitive to the process mean shift (the details are omitted here but are available from the authors). Hence we can use this chart to check whether the process mean and covariance are in-control simultaneously. The major drawback is that when  $MCD_1(0)$  gives a signal, it is difficult to distinguish a mean shift from a covariance change. To control the process mean and covariance separately, a commonly used method is to form a subgroup of observations at each time period to reduce the effects of the process mean shift on the chart of covariance. The major difference between our chart and the traditional ones is that in our chart a small sample size is allowed, while the speed of detecting covariance changes is maintained.

### Case 2: Using subgroups

Let  $x_{ik}, 1 \leq k \leq n$ , be a subgroup of observations in the *i*-th time period. Assume that  $x_{ik}, 1 \leq k \leq n, i \geq 1$  are i.i.d. and follow *p*-dimensional normal with mean  $\mu_i$  and covariance  $\Sigma$ . Let  $\Sigma_0$  be the nominal value of  $\Sigma$  estimated from the previous samples. In this case, the principle for constructing a CUSUM control chart is the same as in Case 1, and so we omit the details. This chart is denoted by  $MCD_n(0)$ .

#### 2.2. Likelihood Ratio Approach

Roy's statistic can be used to construct a Shewhart chart, namely SR (see Appendix III for the definition). The commonly adopted method to improve the performance of a Shewhart chart is to apply the CUSUM procedure to the statistics used in that chart (for example, Roy's statistics in the SR chart). Especially, a CUSUM version of the SR chart is obtained in this way. The PP based CUSUM chart for covariance turns out to be a procedure based on Roy's statistics of cumulative sample covariance matrices. The important difference between the above two CUSUM charts lies in the order of applying the CUSUM and Roy procedures. In the PP based CUSUM chart we first calculate the cumulative sample covariance matrices and then apply Roy's procedure while in the CUSUM version of the SR chart we first apply Roy's procedure. The principles mentioned in the last subsection support that the CUSUM procedure should be applied before Roy's procedure. It is natural to apply the likelihood ratio procedure SA, instead of SR, to these cumulative sample covariance matrices (see Appendix III for the definition of the SA procedure). That is, for n > p

and  $1 \le j < i$ , let

$$S_{ij} = (i - j + 1)(n - 1)(-p - \log(\det(V_{ij})) + tr(V_{ij}))$$

where  $V_{ij}$  is defined by

$$\{(y_{i1}y_{i1}^{\top} + \dots + y_{in}y_{in}^{\top})/(n-1) + \dots + (y_{i1}y_{i1}^{\top} + \dots + y_{in}y_{in}^{\top})/(n-1)\}/(i-j+1),$$

and  $det(\cdot)$  and  $tr(\cdot)$  denote the determinant and trace of a square matrix. And let

$$S_i = \max\{0, S_{i1}, \cdots, S_{ii}\}.$$

Then a new CUSUM chart, named  $LRC_n$ , can be defined to indicate an out-of-control message when  $S_i > h$ , where h is the control limit.

Note that according to the likelihood ratio procedure, the factor n-1 in  $S_{ij}$  and  $V_{ij}$  above should be n. The corresponding procedure is called  $LCR'_n$ . In  $LCR_n$  we use the unbiased sample covariance estimator unlike  $LCR'_n$  where the maximum likelihood estimator of covariance is used. See Alt and Smith (1988, p. 344).  $LCR'_n$  is a biased procedure in the sense that some out-of-control ARLs may be larger than the in-control ARL. So it is not surprising that the simulation in Table 2.1 indicates that  $LCR_n$  is significantly better than  $LCR'_n$ . We recommend using the  $LCR_n$ .

# 3. Procedure of Constructing the New Charts

First we consider the case that the nominal value  $\Sigma_0$  is known or can be estimated by the previous in-control samples. The other cases will be discussed in the next section. The procedure of  $MCD_1(0)$  involves the following steps.

Step 1: Determine the parameters in  $MCD_1(0)$ . Choose  $k_u$  and  $k_l$ , for example,  $k_l = 0.5$  and  $k_u = 1.5$ . The parameters  $h_l = -h$  and  $h_u = h$  are determined by the values of in-control ARL (average run length) and SRL (standard deviation of run length) which are specified in advance (see Tables 5.1, 5.2). Alternatively, h is specified first and the ARL and SRL values are then determined.

Step 2: For each i, calculate the sample average  $\bar{x}_i$  of  $x_{ik}$ ,  $1 \leq k \leq n$  and make the following transformation on  $x_{ik}$ ,

$$y_{ik} = \Sigma_0^{-1/2} (x_{ik} - \bar{x}_i) \text{ for } n > 1;$$

$$y_{i1} = \Sigma_0^{-1/2} (x_{i1} - \mu_0)$$
 for  $n = 1$ .

Step 3: Calculate  $SU_i$  and  $SL_i$ . For each i and  $1 \le j \le i$ , first calculate the maximum and the minimum eigenvalues and the corresponding eigenvectors of

$$(y_{j1}y_{j1}^{\top} + \dots + y_{jn}y_{jn}^{\top})/(n-1) + \dots + (y_{i1}y_{i1}^{\top} + \dots + y_{in}y_{in}^{\top})/(n-1), \text{ for } n > 1$$
  
$$y_{j1}y_{j1}^{\top} + \dots + y_{i1}y_{i1}^{\top}, \text{ for } n = 1.$$

They are denoted by  $\lambda_{ij}^u$ ,  $e_{ij}^u$  and  $\lambda_{ij}^l$ ,  $e_{ij}^l$ . Then we calculate

$$SU_{ij} = \lambda_{ij}^{u} - (i - j + 1)k_{u}, \quad SL_{ij} = \lambda_{ij}^{l} - (i - j + 1)k_{l}$$

followed by

$$SU_i = \max\{0, SU_{i1}, \dots, SU_{ii}\}, \quad SL_i = \min\{0, SL_{i1}, \dots, SL_{ii}\}.$$

Let u(i) and l(i) be such that  $SU_{iu(i)} = SU_i$  and  $SL_{il(i)} = SL_i$ .

Step 4: Check whether  $SU_i$  is above  $h_u$  and whether  $SL_i$  is below  $h_l$ . If  $SU_i > h_u$ , then a upward change signal of  $\Sigma$  in direction  $e^u_{iu(i)}$  is indicated. If  $SL_i < h_l$ , then a downward change signal of  $\Sigma$  in direction  $e^l_{il(i)}$  is indicated.

Like in the CUSUM chart for the process mean (see, for example, Hawkins and Olwell, 1998, p. 20–21), we can give an estimate of when the change occurs when  $SU_i$  or  $SL_i$  falls outside the control limits. We look backward from the period i to check the subgroups:  $x_{jk}$ ,  $1 \le k \le n, 1 \le j \le i$ . Similar to the CUSUM chart for the process mean, if  $SU_{ij}$  falls outside the control limits, then we predict that the change occured at a period not later than j.  $SU_{ij}$  shows the magnitude of such shift (see Appendix II). There may be several such j. It natural to choose the most significant one, namely u(i), in the sense that  $SU_{iu(i)} = \max\{0, SU_{ij}, 1 \le j \le i\}$ .

#### 4. Enhancements of the New Charts

#### 4.1. FIR CUSUM

The fast initial response (FIR) feature is useful when there are start-up problems or ineffective control actions after the previous out-of-control signal (see, Lucas and Saccucci, 1990). The aim of FIR is to reduce the RL for mean shifts that one wishes to detect without significantly reducing the in-control RL. A direct way of achieving this aim is to narrow the control limits. But simulations show that a more efficient way to improve the FIR feature of  $MCD_n(0)$  is to add some time-varying constants to the CUSUM values (the details is available from author). Here we present a method used by Ngai and Zhang (1994). Take  $MCD_n(0)$  as an example. The new CUSUM values are of the forms  $\{SU_i + r^{u(i)+1}h_u\}$  and  $\{SL_i + r^{l(i)+1}h_l\}$ , where  $0 \le r < 1$  and u(i) and v(i) are defined in Section 2.1. Using the same control limits of  $MCD_n(0)$  and the new sequences of the CUSUM values, we can define a FIR CUSUM chart, denoted by  $MCD_n(r)$ . For the simplicity of notion, the new sequences of the CUSUM values are still denoted by  $\{SU_i\}$  and  $\{SL_i\}$ .

The spirit of this improvement can be illustrated as follows. When the process is in-control, most CUSUM values should be around zero and relatively far away from the control limits. Hence, if we add a small value to each CUSUM value, the new sequences of CUSUM values will be still within the control limits. On the contrary, when the process is out-of-control, the CUSUM sequence will tend to the control limits and then fall outside the control limits. If we add a small value to each CUSUM value, the new sequence of CUSUM values will fall outside the control limits more

quickly. As a result, a shorter out-of-control RL is obtained. The reason why we choose  $r^{u(i)+1}h_u$  and  $r^{l(i)+1}h_l$  as the values to be put in the i-th CUSUM values is the following. Note that  $SU_i \leq h_u$  is equivalent to  $SU_{ij} \leq h_u$ ,  $1 \leq j \leq i$ . This implies that for the fixed i, the upper control limit for  $SU_{ij}$ ,  $1 \leq j \leq i$  is a constant. Motivated by the sequential theory (for example, Siegmund, 1986), we can improve the performance of the chart by replacing the constant control limit by some exponential control limit  $(1-r^{j+1})h_u$ , which varies in j. Now the corresponding upper control limit for  $SU_{iu(i)}$  is  $(1-r^{u(i)+1})h_u$ . For simplicity, we check only whether  $SU_{iu(i)} > (1-r^{u(i)+1})h_u$  (which is equivalent to  $SU_{iu(i)} + r^{u(i)+1}h_u > h_u$ ). A similar illustration can be found for  $r^{l(i)+1}h_l$ .

### 4.2. No Previous in-Control Samples

In some situations, the nominal values of  $(\mu_0, \Sigma_0)$  are usually unknown at the beginning. We need to modify  $MCD_1(r)$  by the following commonly used method: during the *i*-th period, we use the sample average and covariance  $\hat{\mu}_{i-1,0}$  and  $\hat{\Sigma}_{i-1,0}$  of the first i-1 samples to estimate  $\mu_0$  and  $\Sigma_0$  if no signal appears at the first i-1 periods. For the singular sample covariance  $\hat{\Sigma}_{i-1,0}$ ,  $\hat{\Sigma}_{i-1,0}^{-1/2}$  is defined as the generalized inverse of  $\hat{\Sigma}_{i-1,0}^{1/2}$ .

# 5. RL Performances and Designs of the New Charts

# 5.1. RL Performances

The performance of a control chart to detect process change when it is out-of-control is evaluated by its RL. The RLs of  $MCD_n(r)$ ,  $LCR'_n$  and  $LRC_n$  have two Properties (see Appendix IV for the proof):

- (i) The distribution of RL depends just on the solutions of the equation  $det(\Sigma \lambda \Sigma_0) = 0$ , where  $\Sigma_0$  is the nominal value of the process covariance when it is in-control and  $\Sigma$  is the real value of the process covariance.
- (ii) The distributions of the RLs of  $MCD_1(r)$  and  $MCD_2(r)$  are the same provided that they have the same parameters  $k_u$ ,  $k_l$ , p,  $h_u$  and  $h_l$ , and the underlying process is normally distributed.

Property (i) also holds for the Shewhart charts: SA, SA', SR and SV defined in Appendix III. Let  $\Sigma_1$  and  $\Sigma_2$  be two covariance matrices such that  $\Sigma_0^{-1/2}\Sigma_1\Sigma_0^{-1/2}$  is diagonal with the same eigenvalues as  $\Sigma_0^{-1/2}\Sigma_2\Sigma_0^{-1/2}$ . Observe that the equations,  $det(\Sigma_1-\lambda\Sigma_0)=0$  and  $det(\Sigma_2-\lambda\Sigma_0)=0$ , have the same solution in this setting. Then, by Property (i), the distributions of the RLs with  $\Sigma_1$  and  $\Sigma_2$  are the same. Thus, when we examine the out-of-control performance, we need only to consider the situation when  $\Sigma_0^{-1/2}\Sigma\Sigma_0^{-1/2}$  is diagonal with the i-th elements being the eigenvalues of  $\Sigma_o^{-1/2}\Sigma\Sigma_o^{-1/2}$ . This makes the performance evaluation of  $MCD_n(r)$ , SA', SA, SR, SV,  $LCR'_n$  and  $LRC_n$  easier.

Although the RL distribution of  $MCD_1(r)$  and  $MCD_2(r)$  are the same, the assumptions behind  $MCD_1(r)$  and  $MCD_2(r)$  are different. In the former we assume  $\mu = \mu_o$  is known and sample size is 1. In the latter we do not assume  $\mu$  is known. So the process mean can be either in-control or

out-of-control. But we assume there is the additional information that the sample size is 2 in each time period. This information is used for estimating the unknown parameter  $\mu$ .

# 5.2. Designs of the FIR Parameter

Traditionally, we use the average RL (ARL) to summarize the main feature of an RL. However, in some situations, it may be misleading. For instance, most authors have adopted the following strategy in designing a control chart: choose the parameters in the chart so that the out-of-control ARL's are as small as possible, subject to the in-control ARL being larger than or equal to some specified number. Unfortunately, for the exponentially weighted moving average chart (EWMA) with time-varying control limits (see Lowery et el. 1992) or  $MCD_n(r)$  discussed in this paper, we can choose the parameters so that the out-of-control ARL's are extremely small (near 1) while the in-control ARL is still larger than that specified number. However, the variances of in-control RL are tending to infinity. This will result in a lot of extremely small RL observations even if the process is in-control (see Chan and Zhang, 1997, for details). So when we evaluate the performance of a chart, we need to calculate ARL as well as the standard deviation of RL (SRL). Furthermore, when we select the parameter r, we must put some constraint on the coefficient of variation of the RL.

Recently, Chan and Zhang (1997) suggested as a constraint that the coefficient of variation of RL should be designed to be smaller than or close to 1. We use the Shewhart type chart to illustrate the suggestion. For the Shewhart type chart, when a precess is in-control ARL = 1/P and SRL =  $ARL\sqrt{1-P}$  (see Ryan, 1989, p.144), where P is the probability that the test statistic used in that chart will fall outside the control limits. So the coefficient of variation  $SRL/ARL = \sqrt{1-P} \le 1$ . We use this constraint when we design the parameter r of  $MCD_n(r)$ .

There is another problem that we must consider in evaluating the performance of the proposed charts. Ideally, we should calculate all of the out-of-control ARL and SRL when we evaluate the performance of  $MCD_n(r)$  and  $LRC_n$ . However, it is impossible to carry out this task using the Monte Carlo simulation as there are a lot of out-of-control cases. A commonly used approach is to select some typical out-of-control matrices. Recall in Subsection 5.1 that for  $MCD_n(r)$  and  $LRC_n$  with the nominal  $\Sigma_0$ , we need only to select some typical out-of-control matrices from all the  $\Sigma$  with  $\Sigma_0^{-1/2}\Sigma\Sigma_0^{-1/2}$  being diagonal. For each p=2 we select nine typical out-of-control matrices:

$$\Sigma = \Sigma_0^{1/2} T \Sigma_0^{1/2}, \lambda(T) = B_2, C_2, D_2, E_2, F_2, G_2, H_2, J_2, K_2$$

where  $\lambda(T)$  stands for the vector of the eigenvalues of T and

$$\begin{split} B_2 &= (1.5, 0.5), \quad C_2 = (1.25, 0.75), \quad D_2 = (1.5, 1.1), \\ E_2 &= (4.3, 1.), \quad F_2 = (1.5, 1.2), \quad G_2 = (1.1, 1.2), \\ H_2 &= (0.9, 1.2), \quad J_2 = (0.1, 2.5), \quad \text{and} \quad K_2 = (2.5, 3.5). \end{split}$$

 $B_2$ ,  $D_2$ ,  $F_2$ ,  $C_2$ ,  $G_2$ , and  $G_2$  represent some typical moderate or small changes; and  $G_2$ ,  $G_2$  and

 $K_2$  are the examples of large changes. Similarly, for p=3, we select the typical out-of-control matrices  $\Sigma$  with  $\Sigma_0^{-1/2}\Sigma\Sigma_0^{-1/2}$  having the vectors of the eigenvalues:  $B_3$ ,  $C_3$ ,  $D_3$ ,  $E_3$ ,  $E_3$ , and  $E_3$ , respectively, where

$$B_3 = (1.5, 1., 1.),$$
  $C_3 = (1.2, 1.3, 1.),$   $D_3 = (4.5, 3., 2.),$   $E_3 = (0.1, 0.2, 0.5),$   $F_3 = (0.1, 2.5, 0.5),$  and  $G_3 = (0.5, 1.5, 1.).$ 

For each typical case, the out-of-control ARL and SRL are calculated by the Monte Carlo simulation. The replicate number in all of these Monte Carlo simulations is 6,000 or 12000.

In the following cases, as will be shown in Table 5.1, we first select FIR parameter r for  $MCD_n(r)$ . The h is calculated by some pre-determined in-control ARL and SRL (corresponding to  $\Sigma_0$ ). The out-of-control ARL and SRL are then simulated (corresponding to  $B_2$ ,  $C_2$ ,  $D_2$ , and  $E_2$ ). For illustration purpose, the in-control ARL and SRL are chosen to cover various r and h values within certain ranges.

#### Case 1: n = 1 or n = 2.

For  $p=2, k_u=1.5$  and  $k_l=0.5$ , the ARL and SRL of  $MCD_1(r)$  with r=0,0.3,0.6,0.8 are shown in Table 5.1. It suggests that for p=2, r=0.6 has a better ability to detect the process covariance change among  $MCD_1(r), 0 \le r < 1$ , subject to the condition that the coefficient of variation of the RL is close to 1. If we prefer a chart with a small coefficient of variation, r=0 is a good choice. Note that, as pointed out in Subsection 5.1 (ii), the above result also holds for n=2.

# Case 2: n = 5.

For p = 2,  $k_u = 1.5$  and  $k_l = 0.5$ , the ARL and SRL of  $MCD_5(r)$  with r = 0.0, 0.4, 0.5, 0.6 are given in Table 5.1. Making a comparison of these numerical results, we suggest that any value between 0.4 and 0.6 is a reasonable choice for r.

# Case 3: n = 10.

For p = 2,  $k_u = 1.5$  and  $k_l = 0.5$ , the ARL and SRL of  $MCD_{10}(r)$  with r = 0.0, 0.3, 0.45 and 0.6 are shown in Table 5.1. Any value between 0.3 and 0.45 seems to be a reasonable choice for r. Note that, for p = 3 and 4, the results are similar and not shown here.

In summary, for fixed n, p and control limits, as r tends to 1, the ARL of the chart decreases while the SRL of the chart increases. For fixed n and p, it is possible to adjust  $0 \le r < 1$  and control limits so that the in-control ARL is not less than some specified level, the out-of-control ARL is as small as possible and the coefficient of variation of RL is below or close to 1.

In-control ARL and SRL are two important quantities in selecting a chart. The in-control ARL and SRL of  $MCD_1(0.6)$ ,  $MCD_1(0)$ ,  $MCD_2(0)$ ,  $MCD_2(0.6)$ ,  $MCD_5(0)$ ,  $MCD_{10}(0)$ ,  $LRC_5$  and  $LRC_{10}$  under various control limits h are listed in Tables 5.2 and 5.3.

# 6. Applications to Paired Measurements

Grubbs's model is used for assessing bias and precision of paired measurement systems (see Blackwood and Bradley 1991). We employ this model to account for the bias and variation of observed measurements of a process. For simplicity, we will consider only the systems with two devices being used to measure a process. Then Grubbs's model is of the form

$$x_{i1} = \mu + d_i + \alpha_1 + \epsilon_{i1}, \quad x_{i2} = \mu + d_i + \alpha_2 + \epsilon_{i2}, \quad i \ge 1,$$
 (6.1)

where  $x_{ij}$  is the observed measurement when the *i*-th specimen is measured with the *j*-th device,  $j=1,2,\mu$  is the hidden (or true) process mean,  $d_i$  is the true random deviation of the process from  $\mu$  for the *i*-th specimen;  $\alpha_j$  is the bias for device j, and  $\epsilon_{ij}$  is the random error for the *i*-th specimen when measured by device j. In practice the variation observed from a process is due to the hidden process variability and the error of the measurement device. If we use only single device to measure a process, it is impossible to account for the sources when an out-of-control signal appears. We will show that if two devices are used, a synthetic chart can be plotted for the variations of two devices as well as for the process variance. A similar chart can also be plotted for the relative precision—the ratio between the hidden process variance and the total observed variance. To this end, we first formulate the above model in terms of the multivariate statistical analysis. Let

$$\mu_i = (\mu + \alpha_1, \mu + \alpha_2)^{\top}, \quad \epsilon_i = (\epsilon_{i1}, \epsilon_{i2})^{\top}$$

 $dd_i = (d_i, d_i)^{\top}$  and  $x_i = (x_{i1}, x_{i2})^{\top}$ . Then model (6.1) is equivalent to

$$x_i = \mu_i + dd_i + \epsilon_i, \quad i \ge 1.$$

Assume that, given  $dd_i$ , the expectations of  $\epsilon_i$  and  $\epsilon_{i1}\epsilon_{i2}$  are zero. Let  $\sigma_d^2$ ,  $\sigma_{\epsilon_1}^2$  and  $\sigma_{\epsilon_2}^2$  are the variances of the process and the devices. Under these assumptions, the covariance matrix of  $x_i$  is

$$\left( \begin{array}{cc} \sigma_d^2 + \sigma_{\epsilon_1}^2 & \sigma_d^2 \\ \sigma_d^2 & \sigma_d^2 + \sigma_{\epsilon_2}^2 \end{array} \right)$$

and the relative precision of the process is  $\sigma_d^2/\sqrt{(\sigma_d^2+\sigma_{e_1}^2)(\sigma_d^2+\sigma_{e_2}^2)}$ .

The covariance of  $x_i$  changes if the process variance or one of device variances changes. Hence, to control the process variance or the measurement variance of the devices, it is sufficient to control the covariance of the multivariate variable  $x_i$ . Similarly, to control the relative precision, it suffices to control the correlation of paired measurements.

Example 6.1. This example involves a real bivariate data set used by Tracy, Young and Mason (1995, P. 374). The data set contains 19 paired measurements from a petrochemical industry. The first 15 observations are taken from a stable process and used to estimate the in-control  $\mu_0$  and  $\Sigma_0$ . The results are

$$\hat{\mu}_0 = (7.09, 7.113)$$
 and  $\hat{\Sigma}_0 = \begin{pmatrix} 0.1498 & 0.0334 \\ 0.0334 & 0.0241 \end{pmatrix}$ 

Tracy, Young and Mason (1995) applied the partial  $T^2$ -Shewhart control chart for the process mean to this data set and demonstrated that the observations 18 and 19 indicate that the process mean is out-of-control (the referee pointed out that the partial  $T^2$  statistics are not independent and F distributed as Tracy, Young and Mason claimed). They showed that the obervations 18 and 19 are located at the opposite regions (see Figure 3 in Tracy, Young and Mason, 1995). In our opinion the locations of the observations 18 and 19 implies the process covariance, not the process mean, is changed. This is because if the process mean is changed and the covariance is in-control, the following observations should be not far from each other. Here we use  $MCD_2(0.6)$  to support our view. Now paired measurements 16 through 19 are used to check whether the hidden process variance and the device variances are in control. To reduce the effect of the process mean, these four paired measurements are grouped into two samples. Then these two samples are monitored by  $MCD_2(0.6)$ . From Table 5.2, with  $k_u = 1.5$ ,  $k_l = 0.5$  and h = 12, the in-control (ARL, SRL) is (130, 128). The CUSUM values are  $SU_1 = 6.88$ ,  $SL_1 = -4.83$ ,  $SU_2 = 107.4$  and  $SL_2 = -4.95$ .  $SU_2$  falls outside the upper control limit. Therefore, an out-of-control signal appears at the second subgroup. The other CUSUM values are within the control limits. Thus both the hidden process variance and the variances of measurement system are in control at the first subgroup.

### 7. Illustrative Examples

The following two examples show that  $MCD_1(r)$  can be used when both  $\mu_0$  and  $\Sigma_0$  are known or can be estimated from the previous samples.  $MCD_1(r)$  can detect both changes in the process mean and covariance. However, when we obtain an out-of-control signal, it is difficult to determine whether the signal is due to change of the process covariance or the process mean.

**Example 7.1.** We begin with 28 samples of size 1 (see Table 7.1). The first two samples are drawn from a three-dimensional normal  $N(0, I_3)$ , while the remains of samples are drawn from a three-dimensional normal N(0, G) with

$$G = \left(\begin{array}{ccc} 1.5 & -0.5 & -0.5 \\ -0.5 & 1.5 & -0.5 \\ -0.5 & -0.5 & 1.5 \end{array}\right).$$

We use  $MCD_1(0)$  and the FIR chart  $MCD_1(r)$  to detect the covariance change in this data set. First, we use  $MCD_1(0)$ .

Step 1: Select suitable parameters for  $MCD_1(0)$ . We choose  $k_u = 1.5$ ,  $k_l = 0.5$  and h = 15. The in-control (ARL,SRL) is then (118, 109) obtained by simulation.

Step 2: Calculate  $y_i$  by multiplying each sample by  $\Sigma_0^{-1/2}$ . In this example  $x_i = y_i$ .

Step 3: Calculate the CUSUM values,  $SU_i$  and  $SL_i$ , and u(i) and l(i).

Step 4: Check whether  $SU_i$  or  $SL_i$  falls outside the control limits. 28 CUSUM values are plotted on the chart in Figure 7.1. It shows that  $MCD_1(0)$  gives an out-of-control signal at the

6-th sample. Note that u(6) can be used to estimate when the covariance change occurs.

Now we use  $MCD_1(r)$  to monitor the same data set. Using  $k_u = 1.5$ ,  $k_l = 0.5$ , p = 3, n = 1, r = 0.6 and h = 15 in Table 5.2, the in-control (ARL,SRL) are (109, 109).  $MCD_1(0.6)$  gives an inflated out-of-control signal at the 3-th sample. So, compared with  $MCD_1(0)$ ,  $MCD_1(0.6)$  has a faster response to an initial change.

In the short-run production environment, to detect the possible covariance change before the end of production process we use the maximum number of observations to truncate the RL of  $MCD_n(r)$ . Example 7.2 illustrates such situation. It shows that, unlike other charts, the proposed chart can be used even where the sample size is smaller than the dimension of process distribution and the process mean varies between samples.

**Example 7.2.** Suppose the maximum number of samples is 71. The first two samples are from a three-dimensional normal  $N(0, I_3)$ , where  $I_3$  is the unit matrix. The remains are from a three-dimensional normal with mean  $(1, -2, -3)^{\top}$  and covariance

$$C = \begin{pmatrix} 2.00 & -0.25 & -0.25 \\ -0.25 & 1.00 & -0.25 \\ -0.25 & -0.25 & 2.00 \end{pmatrix}$$

We use  $MCD_3(0.6)$  truncated by 71 to check whether a change has occurred in the process covariance. Let  $k_u = 1.5$ ,  $k_l = 0.5$ , and h = 13. According to Table 5.2, the in-control ARL is 42 (< 71). Calculate and plot the CUSUM values on the chart. An inflated out-of-control signal appears at the fourth sample (see Figure 7.2). In practice we may not want to stop the process immediately when an out-of-control signal appears in order to obtain some additional samples to estimate the magnitude of the change. As an example, here we stop the process after we obtained 10 additional out-of-control samples.

#### 8. Comparison with other charts

In this section, using the Monte Carlo simulation, the performance of the proposed charts is compared with the following charts. The definitions of these charts are given in Appendix III. The replicate number in this study is 6000 or 12000, as before.

- 1. SR chart—the Shewhart chart based on Roy's maximum and minimum eigenvalues of sample variances (see Anderson 1984, p. 328).
  - 2. SA chart—the Shewhart chart based on Anderson's test of covariance (see Alt 1988, p. 344).
- 3. SV chart—the Shewhart chart based the square root of Hotelling's generalized variance (see Alt 1988, p. 349).

Note that the sample size n > p is required in all of these Shewhart type charts. We take n = 5 and p = 2, 3 in this study.

Table 8.1 shows the results of the comparison of these charts with the  $MCD_5(0)$  (with  $k_u = 1.5$  and  $k_l = 0.5$ ) and  $LRC_5$  chart for p = 2,3 when n = 5. It is clear from these comparisons that the SA and SR charts are more effective than the SV chart in detecting the process covariance change. Compared with the SA, SR and SV charts, in many cases  $MCD_5(0)$  and  $LRC_5$  can detect the moderate or small covariance change more than twice faster. The SR chart is slightly better than  $MCD_5(0)$  and  $LRC_5$  in detecting the relatively larger covariance change such as  $E_2$ . It is found that  $MCD_5(0)$  with  $k_u = 1.5$  and  $k_l = 0.5$  can perform better than  $LRC_5$  when only upward changes exist (for example,  $E_2$  and  $E_2$ ) and worse than  $E_3$  when a certain amount of downward changes happen (for example,  $E_3$  and  $E_3$ ). It is clear that by adjusting the reference values we can make  $E_3$ 0 more sensible to some pre-specified change at the cost of effectiveness for detecting some other changes.

As pointed out in Hawkins and Olwell (1997, p. 87, 144-145), in one dimensional cases, the sample variance of each subgroup has a  $\chi^2$  distribution (which belongs to the gamma family). By applying the likelihood ratio procedure to the gamma distribution, they showed that if the Johnson-Leone CUSUM chart is used to monitor for an increasing in variance from the in-control standardized variance 1 to a larger variance  $\sigma_u^2$  or to a smaller variance  $\sigma_l^2$ , the optimal reference values should be

$$k_u = \sigma_u^2 log(\sigma_u^2) / (\sigma_u^2 - 1), \quad k_l = \sigma_l^2 log(\sigma_l^2) / (\sigma_l^2 - 1).$$

For example, if  $\sigma_u^2 = 1.5$  and  $\sigma_l^2 = 0.5$ , we recover the frequently used reference values  $k_u = 1.5$ and  $k_l = 0.5$  approximately. However, in multivariate cases, neither the largest nor the smallest eigenvalues of the sample covariance matrix of each subgroup follows the  $\chi^2$  distribution (see Muirhead, 1982, p. 420-425). This implies that the above formulae for  $k_u$  and  $k_l$  may be not optimal for the multivariate cases from the point view of the likelihood ratio. This suggests that it may be possible to improve the performance of  $MCD_n(0)$  and SR by choosing suitable  $k_u$  and  $k_l$  or pair values of  $(h_l, h_u)$ . Unfortunately it is time-consuming if we try to directly optimize  $MCD_n(0)$ with respect to  $k_u$  and  $k_l$ . Here we find a relatively fast but empirical way to adjust the reference values to improve the performance of  $MCD_5(0)$ , substantially, in detecting the downward changes. It is based on the following observation: although  $MCD_5(0)$  with  $k_u = 1.5$  and  $k_l = 0.5$  is very fast for detecting the upward changes, it is very slow when some downward changes happen. For example, the out-of- control ARLs for some downward changes could be larger than the in-control ARL. In the word of test, this means that like  $LCR'_5$ ,  $MCD_5(0)$  with  $k_u = 1.5$  and  $k_l = 0.5$  is biased. The simulation in Table 8.2 shows that we can use the following method to choose the reference values so that the resulting  $MCD_5(0)$  is unbiased, that is, the out-of-control ARLs are less than the in-control ARL: First, we set  $k_u = 1.5$ ,  $k_l = 0.5$  and  $h = h_o$ . Then we choose  $c_o > 0$ such that  $ARL(c_o) = \max_{c>0} ARL(c)$ , where ARL(c) is the out-of-control ARL when  $\Sigma = c\Sigma_o$ . Now if let  $k_u = 1.5/c_o$ ,  $k_l = 0.5/c_o$  and  $h = h_o/c_o$ , then the corresponding ARL(c) for the new  $MCD_n(0)$  attains the maximum at c = 1. In Table 8.2 we demonstrate that the performance of  $MCD_5(0)$  with the adjusted reference values are now very similar to the  $LCR_5(0)$  which can detect the upward changes as well as the downward changes fast.

# 9. Conclusions

We have proposed CUSUM charts  $MCD_n(r)$  and  $LRC_n$  for monitoring the change of the covariance matrix of a multivariate normal process using the projection pursuit and likelihood ratio respectively.  $MCD_n(r)$  is a natural extension of the CUSUM chart of Johnson and Leone (1962) for variance while  $LRC_n$  is not.

The distribution of the run lengths of the control charts  $MCD_n(r)$  and  $LRC_n$  depend on the nominal value  $\Sigma_0$  and the actual  $\Sigma$  of the process only and is through the characteristic roots of the equation  $det(\Sigma - \lambda \Sigma_0) = 0$ .

Unlike the Shewhart type or likelihood ratio based charts, of which the subgroup size n is required to be at least equal to the dimension p, the PP based CUSUM charts can be used for any size  $n \geq 1$ . In Table 9.1, we present some out-of-control ARLs of  $MCD_2(0)$  with p = 3 to show that  $MCD_2(0)$  still has a good performance when the sample size is less than the dimension of the the quality characteristics.

Simulation studies on the ARL and SRL indicate that a considerable improvement on the other three charts in terms of faster detection of the covariance change can be achieved if  $MCD_n(r)$  (or  $LRC_n$ ) is used. However, the former calculation is more complicated.

Several simulated examples are given to illustrate the use of the proposed chart.  $MCD_n(r)$  is also applied to the monitoring of the process variability and measurement errors in paired measurements systems.

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# Appendix I

The proof of Principles (i) and (ii) in Section 2.

To prove (i), we note that the variances of  $a_{max}^{\top} \Sigma_0^{-1/2} X$  and  $a_{min}^{\top} \Sigma_0^{-1/2} X$  are

$$a_{max}^{\top} \Sigma_0^{-1/2} \Sigma \Sigma_0^{-1/2} a_{max} = \max_{||a||=1} a^{\top} \Sigma_0^{-1/2} \Sigma \Sigma_0^{-1/2} a$$

and

$$a_{min}^{\top} \Sigma_0^{-1/2} \Sigma \Sigma_0^{-1/2} a_{min} = \min_{\|a\|=1} a^{\top} \Sigma_0^{-1/2} \Sigma \Sigma_0^{-1/2} a$$

respectively. Hence, the variances of  $a_{max}^{\top} \Sigma_0^{-1/2} X$  and  $a_{min}^{\top} \Sigma_0^{-1/2} X$  is equal to 1 if and only if

$$\max_{||a||=1} a^{\top} \Sigma_0^{-1/2} \Sigma \Sigma_0^{-1/2} a = \min_{||a||=1} a^{\top} \Sigma_0^{-1/2} \Sigma \Sigma_0^{-1/2} a = 1,$$

which holds if and only if  $\Sigma_0^{-1/2}\Sigma\Sigma_0^{-1/2}$  is an identity matrix, that is,  $\Sigma_0=\Sigma$ .

The proof of (ii) is similar.

# Appendix II

Consider  $SU_i^a$ . We want to prove that as  $v \to \infty$ 

$$SU_n^a/v \to E(a^\top X)^2 - k_u$$

in probability when  $E(a^{\top}X)^2 > k_u$ . In fact, if we define

$$w_0 = 0, \quad w_m = \sum_{j=1}^m ((a^{\top} x_j)^2 - k_u), \quad m \ge 1,$$

then

$$SU_m^a = \max\{0, w_m - w_{m-1}, w_m - w_{m-2}, \cdots, w_1 - w_0\}.$$

Suppose  $E(a^{\top}x_i)^2 = 1, i = 1, \dots, m_0$ , and  $E(a^{\top}x_i)^2 = \sigma_a^2, i = m_0 + 1, \dots$ , with  $\sigma_a^2 > k_u$ . Then

$$w_i = \sum_{j=m_0+1}^{i} ((a^{\top} x_j)^2 - k_u) + \sum_{j=1}^{m_0} ((a^{\top} x_j)^2 - k_u).$$

According to the convergence theory of stochastic process (see Pollard, 1984, p106), as  $v \to \infty$ , we have

$$w_i/v = (\sigma_a^2 - k_u)i/v + o_p(1)$$

where  $o_p(1)$  is uniform for  $1 \leq i \leq v$ . Hence for large v

$$SU_v^a/v = \max\{0, (\sigma_a^2 - k_u)(1 - 1/v), \cdots, (\sigma_a^2 - k_u)(1 - v/v)\} + o_p(1)$$
  
=  $\sigma_a^2 - k_u + o_p(1)$ 

when  $\sigma_a^2 > k_u$ . The proof is completed.

#### Appendix III

Here we give the definitions of the SR, SA and SV charts and their RL performances. As in Section 3, we first make a transformation of each  $x_{ij}$  into  $y_{ij}$  by multiplying  $\Sigma_0^{-1/2}$ ,  $1 \leq j \leq i$ . Let  $s^2(y_i) = \sum_{j=1}^n (y_{ij} - \overline{y}_i)(y_{ij} - \overline{y}_i)^\top/(n-1)$  be the sample covariance of the *i*-th transformed sample, where  $\overline{y}_i = \sum_{j=1}^n y_{ij}/n$ .

SR Chart. Let  $SR_{ui}$  and  $SR_{li}$  denote the maximum and minimum eigenvalues of  $s^2(y_i)$ ,  $C_{ur}$  and  $C_{lr}$  be the upper and lower control limits, and  $k_u$  and  $k_l$  be the upper and lower reference values. In this paper, we choose  $k_u = 1.5$  and  $k_l = 0.5$  as those for  $MCD_5(0)$ . Then, the SR chart is defined to indicate an out-of-control signal when  $SR_{ui} - k_u > C_{ur}$  or  $SR_{li} - k_l < C_{lr}$ . Here, we choose  $C_{ur} = -C_{lr} = h$ , and h is a positive constant.

SA Chart. Suppose n > p. Let

$$SA_i = (n-1)(-p - \log(\det(s^2(y_i))) + tr(s^2(y_i))),$$
  

$$SA'_i = n(-p - \log(\det((n-1)s^2(y_i)/n)) + tr((n-1)s^2(y_i)/n))$$

where  $det(\cdot)$  and  $tr(\cdot)$  denote the determinant and trace of a square matrix. Then the SA chart is defined to give an out-of-control signal when  $SA_i > h$ . Here, without confusion, h denotes the upper control limit of the SA chart. Similarly, the SA' chart is defined by using  $SA'_i$ .

SV Chart. Suppose n > p. Let

$$SV_i = (\sqrt{\det(s^2(y_i))} - b_3) / \sqrt{b_1 - b_3^2},$$

where  $b_1 = (n-1)^{-p} \prod_{k=1}^p (n-k)$ ,  $b_3 = (2/(n-1))^{p/2} \Gamma(n/2)/\Gamma((n-p)/2)$ , and  $\Gamma(\cdot)$  is the Gamma function. Then, the SV chart is defined to indicate an out-of-control signal when  $SV_i$  falls outside the upper and lower control limits  $C_{ur}$  and  $C_{lr}$ . Usually we choose  $C_{ur} = -C_{lr} = h$ , where h is a positive constant.

# Appendix IV

Property (i) directly follows from the definitions of  $MCD_n(r)$  and  $LRC_n$ .

To prove Property (ii), we first let n=2 and

$$y_k^* = (x_{k1} - x_{k2})/\sqrt{2}, k = 1, 2, \cdots$$

Then,

$$(y_{j1}y_{j1}^{\top} + \dots + y_{jn}y_{jn}^{\top})/(n-1) + \dots + (y_{i1}y_{i1}^{\top} + \dots + y_{in}y_{in}^{\top})/(n-1) = y_i^*y_i^{*\top} + \dots + y_i^*y_i^{*\top}.$$

Note that, under the i.i.d. and normal assumption,  $\{y_k^*, k \geq 1\}$  have the same distributions as  $\{x_{k1} - \mu_o, k \geq 1\}$ . So the distributions of the statistics  $SU_i$  and  $SL_i$  are invariant when we reply  $x_{k1} - \mu_o$  by  $y_{kn}$ . Thus, the RL distributions of  $MCD_1(0)$  and  $MCD_2(0)$  are the same.

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**Table 2.1.** Comparisons of ARL and SRL of SA, SA',  $LCR'_n$  and  $LCR_n$  (with  $k_u=1.5,\ k_l=0.5$ ) charts for  $n=5,\ p=2,3,$  where  $\lambda=\lambda(\Sigma_o^{-1/2}\Sigma\Sigma_o^{-1/2})$ .

|        |      |                      | p =  | $= 2, \mu =$ | : 0  |         |      |                      |
|--------|------|----------------------|------|--------------|------|---------|------|----------------------|
|        | S.   | A'                   | S.   | A            | LC   | $'R'_5$ | LC   | $R_5$                |
|        | h=   | h=20.7               |      | h=16         |      | 60.     | h=1  | 18.6                 |
| λ      | ARL  | $\operatorname{SRL}$ | ARL  | SRL          | ARL  | SRL     | ARL  | $\operatorname{SRL}$ |
| (1, 1) | 203  | 205                  | 203  | 202          | 233  | 67      | 248  | 241                  |
| $B_2$  | 103  | 105                  | 74.1 | 72.2         | 34.0 | 7.98    | 13.0 | 6.28                 |
| $C_2$  | 177  | 179                  | 115  | 115          | 99.2 | 26.1    | 45.2 | 27.5                 |
| $D_2$  | 214  | 216                  | 118  | 114          | 424  | 133     | 32.8 | 20.6                 |
| $E_2$  | 7.72 | 7.03                 | 4.36 | 3.76         | 10.2 | 4.24    | 3.17 | 1.84                 |
| $F_2$  | 220  | 222                  | 74.5 | 73.2         | 582  | 189     | 29.8 | 18.2                 |
| $G_2$  | 232  | 233                  | 185  | 184          | 1232 | 356     | 102  | 73.7                 |
| $H_2$  | 204  | 206                  | 184  | 179          | 220  | 61.6    | 97.1 | 70.9                 |
| $J_2$  | 7.34 | 6.87                 | 5.41 | 4.92         | 6.47 | 1.27    | 2.57 | 0.91                 |
| $K_2$  | 9.81 | 9.24                 | 4.44 | 3.88         | 11.5 | 4.38    | 3.06 | 1.66                 |

|           | $p=3, \mu=0$ |                      |                     |                      |       |                      |      |       |  |  |  |
|-----------|--------------|----------------------|---------------------|----------------------|-------|----------------------|------|-------|--|--|--|
|           | S.           | A'                   | $\operatorname{SA}$ |                      | LC    | $'R'_5$              | LC   | $R_5$ |  |  |  |
|           | h=36         |                      | h=28.25             |                      | h=110 |                      | h=   | 30.   |  |  |  |
| λ         | ARL          | $\operatorname{SRL}$ | ARL                 | $\operatorname{SRL}$ | ARL   | $\operatorname{SRL}$ | ARL  | SRL   |  |  |  |
| (1, 1, 1) | 180          | 181                  | 194                 | 193                  | 212   | 45.5                 | 210  | 198   |  |  |  |
| $B_3$     | 193          | 192                  | 153                 | 150                  | 408   | 86.7                 | 79.7 | 52.4  |  |  |  |
| $C_3$     | 198          | 197                  | 171                 | 168                  | 585   | 127                  | 94.5 | 62.7  |  |  |  |
| $D_3$     | 10.3         | 9.57                 | 13.6                | 12.9                 | 12.9  | 4.0                  | 2.84 | 1.45  |  |  |  |
| $E_3$     | 8.36         | 7.68                 | 3.99                | 3.42                 | 7.33  | 0.96                 | 2.77 | 0.81  |  |  |  |
| $F_3$     | 13.8         | 13.0                 | 12.1                | 11.7                 | 9.38  | 1.43                 | 3.07 | 1.07  |  |  |  |
| $G_3$     | 117          | 117                  | 120                 | 120                  | 48.7  | 8.57                 | 16.1 | 7.2   |  |  |  |

**Table 5.1.** ARL and SDR values of  $MCD_n(r)$  with  $k_u = 1.5$ ,  $k_l = 0.5$ , p = 2 and  $\mu = 0$  when the process is in-control  $(\Sigma_0)$  and out-of-control  $\Sigma$ , where  $\lambda = \lambda(\Sigma_o^{-1/2}\Sigma\Sigma_o^{-1/2})$ 

|        |       |                      | n =      | 1  or  n             | =2     |                      |          |        |
|--------|-------|----------------------|----------|----------------------|--------|----------------------|----------|--------|
| (r, h) | (0.0, | 11.8)                | (0.3, 1) | 11.85)               | (0.6,  | 12)                  | (0.8, 1) | (2.68) |
| λ      | ARL   | $\operatorname{SRL}$ | ARL      | $\operatorname{SRL}$ | ARL    | $\operatorname{SRL}$ | ARL      | SRL    |
| (1, 1) | 129   | 121                  | 130      | 123                  | 130    | 128                  | 130      | 152    |
| $B_2$  | 44.8  | 38.1                 | 44.4     | 38.1                 | 40.9   | 37.7                 | 32.5     | 37.7   |
| $C_2$  | 86.7  | 80.9                 | 87.0     | 81.8                 | 85.7   | 85.9                 | 78.5     | 92.4   |
| $D_2$  | 35.1  | 31.1                 | 34.7     | 31.3                 | 32.3   | 31.8                 | 26.8     | 33.0   |
| $E_2$  | 5.82  | 4.19                 | 5.61     | 4.13                 | 4.84   | 3.98                 | 3.74     | 3.51   |
|        |       |                      |          | n=5                  |        |                      |          |        |
| (r, h) | (0.0, | 3.5)                 | (0.4,    | 3.52)                | (0.5,  | 3.53)                | (0.6,    | 3.54)  |
| λ      | ARL   | $\operatorname{SRL}$ | ARL      | $\operatorname{SRL}$ | ARL    | $\operatorname{SRL}$ | ARL      | SRL    |
| (1, 1) | 104   | 99                   | 105      | 101                  | 104    | 102                  | 102      | 104    |
| $B_2$  | 18.7  | 15.6                 | 17.8     | 15.4                 | 17.1   | 15.3                 | 15.8     | 14.9   |
| $C_2$  | 49.5  | 46.7                 | 48.9     | 47.3                 | 48.2   | 47.7                 | 46.7     | 48.1   |
| $D_2$  | 15.7  | 13.3                 | 14.9     | 13.2                 | 14.3   | 13.2                 | 13.3     | 13.2   |
| $E_2$  | 2.18  | 1.25                 | 2.01     | 1.19                 | 1.92   | 1.14                 | 1.79     | 1.07   |
|        |       |                      | 7        | n = 10               |        |                      |          |        |
| (r, h) | (0.0, | 1.7)                 | (0.3,    | 1.72)                | (0.45, | 1.73)                | (0.6,    | 1.9)   |
| λ      | ARL   | SRL                  | ARL      | $\operatorname{SRL}$ | ARL    | $\operatorname{SRL}$ | ARL      | SRL    |
| (1, 1) | 124   | 122                  | 131      | 129                  | 132    | 132                  | 192      | 202    |
| $B_2$  | 11.8  | 9.50                 | 11.6     | 9.60                 | 11.0   | 9.6                  | 11.1     | 10.5   |
| $C_2$  | 40.1  | 38.0                 | 40.6     | 39.1                 | 40.4   | 39.8                 | 48.6     | 50.2   |
| $D_2$  | 10.4  | 8.80                 | 10.2     | 8.90                 | 9.80   | 8.90                 | 10.0     | 10.0   |
| $E_2$  | 1.36  | 0.61                 | 1.32     | 0.58                 | 1.27   | 0.53                 | 1.22     | 0.50   |

**Table 5.2.** The in-control ARL and SRL of  $MCD_1(0.6)$ ,  $MCD_2(0.6)$ ,  $MCD_1(0)$ ,  $MCD_2(0)$ ,  $MCD_5(0)$  and  $MCD_{10}(0)$  with  $k_u = 1.5$ ,  $k_l = 0.5$  for p = 2, 3, 4 and various control limits h

|      | p=2 |                      |                      | p=3        |     |             | p=4 |     |
|------|-----|----------------------|----------------------|------------|-----|-------------|-----|-----|
|      |     | MCL                  | $O_1(0.6)$           | or         | MCD | $_{2}(0.6)$ |     |     |
| h    | ARL | $\operatorname{SRL}$ | h                    | ARL        | SRL | h           | ARL | SRL |
| 10*  | 45  | 26                   | 13*                  | 42         | 26  | 15*         | 37  | 26  |
| 12   | 130 | 128                  | 15                   | 109        | 109 | 20          | 156 | 159 |
| 15   | 298 | 289                  | 18                   | 231        | 229 | 22          | 242 | 242 |
| 17   | 506 | 489                  | 20                   | 385        | 382 | 23          | 308 | 306 |
| 18   | 642 | 566                  | 22                   | 590        | 538 | 25          | 476 | 456 |
|      |     | МC                   | $\overline{CD_1(0)}$ | or         | MCD | $_{2}(0)$   |     |     |
| h    | ARL | SRL                  | h                    | ARL        | SRL | h           | ARL | SRL |
| 12   | 139 | 133                  | 18                   | 246        | 232 | 22          | 262 | 249 |
| 15   | 309 | 303                  | 20                   | 397        | 370 | 23          | 326 | 306 |
| 17   | 521 | 479                  | 22                   | 610        | 535 | 25          | 498 | 452 |
|      |     |                      | $\Lambda$            | $ICD_5($   | 0)  |             |     |     |
| h    | ARL | SRL                  | h                    | ARL        | SRL | h           | ARL | SRL |
| 3.0* | 43  | 25                   | $4.0^{*}$            | 47         | 25  | $5.0^{*}$   | 45  | 24  |
| 3.5  | 106 | 104                  | 4.5                  | 131        | 129 | 5.5         | 105 | 100 |
| 4.0  | 182 | 178                  | 5.3                  | 302        | 301 | 6.0         | 164 | 162 |
| 4.3  | 249 | 244                  | 5.5                  | 373        | 365 | 6.5         | 257 | 251 |
| 4.5  | 308 | 300                  | 6.0                  | 599        | 535 | 7.0         | 411 | 386 |
|      |     |                      | M                    | $ICD_{10}$ | (0) |             |     |     |
| h    | ARL | SRL                  | h                    | ARL        | SRL | h           | ARL | SRL |
| 1.2* | 32  | 24                   | 1.7*                 | 34         | 24  | 2.3*        | 42  | 25  |
| 1.7  | 123 | 121                  | 2.2                  | 122        | 121 | 2.5         | 89  | 87  |
| 2.0  | 250 | 252                  | 2.5                  | 239        | 237 | 3.0         | 252 | 248 |
| 2.2  | 404 | 389                  | 2.7                  | 374        | 370 | 3.2         | 381 | 371 |
| 2.5  | 760 | 626                  | 3.0                  | 684        | 585 | 3.3         | 465 | 441 |

Note: '\*'—the underlying RL has been truncated by 71.

**Table 5.3.** The in-control ARL and SRL of  $LRC_n$  for (p, n) = (2, 5), (3, 5), (4, 5) and (2, 10), and for various control limits h

| (b   | (n) = (2, | 5)                   | (p.  | (n) = (2, 1) | 10)                  | (p   | (p,n)=(3,5) $(p,n)=(4,5)$ |                      | (p,n)=(4,5) |     |     |
|------|-----------|----------------------|------|--------------|----------------------|------|---------------------------|----------------------|-------------|-----|-----|
| h    | ARL       | $\operatorname{SRL}$ | h    | ARL          | $\operatorname{SRL}$ | h    | ARL                       | $\operatorname{SRL}$ | h           | ARL | SRL |
| 16.8 | 133       | 126                  | 16.0 | 157          | 151                  | 28.8 | 184                       | 180                  | 55.8        | 175 | 174 |
| 17.6 | 174       | 165                  | 16.8 | 210          | 205                  | 29.6 | 225                       | 217                  | 56.6        | 194 | 192 |
| 18.4 | 234       | 229                  | 17.6 | 284          | 280                  | 30.4 | 280                       | 275                  | 57.4        | 217 | 213 |
| 18.6 | 252       | 244                  | 18.4 | 379          | 365                  | 30.8 | 313                       | 307                  | 60.0        | 293 | 282 |
| 19.2 | 308       | 301                  | 19.2 | 507          | 469                  | 31.2 | 347                       | 340                  |             |     |     |
| 20.0 | 415       | 391                  | 20.0 | 679          | 574                  | 32.0 | 419                       | 399                  |             |     |     |

Table 7.1. Simulated data used in Example 7.1

| $x_1$    | $x_2$    | $x_3$    | $x_4$    | $x_5$    | $x_6$    | $x_7$    |
|----------|----------|----------|----------|----------|----------|----------|
| -2.90552 | 0.17469  | 2.17416  | -0.46873 | 1.50455  | 2.84555  | -0.06947 |
| 0.51099  | -0.92729 | -1.74290 | -1.29043 | 1.29883  | -0.57591 | 1.15380  |
| 0.27008  | -1.48665 | -0.61098 | 2.35554  | -0.85250 | 1.01441  | -2.02818 |
| $x_8$    | $x_9$    | $x_{10}$ | $x_{11}$ | $x_{12}$ | $x_{13}$ | $x_{14}$ |
| -1.34906 | -1.70090 | 0.02583  | 1.72567  | 1.66900  | -0.76182 | -0.05649 |
| 0.36748  | 2.47792  | 1.17191  | -0.95384 | -0.60798 | 0.13484  | -1.81073 |
| -1.15512 | -0.88689 | -1.02823 | 0.50284  | -0.91250 | 1.11752  | 0.97035  |
| $x_{15}$ | $x_{16}$ | $x_{17}$ | $x_{18}$ | $x_{19}$ | $x_{20}$ | $x_{21}$ |
| -1.64530 | -1.30068 | -1.69236 | -1.33948 | -0.91634 | -0.85476 | 0.48865  |
| 0.96462  | -0.81295 | 9.26316  | -3.10570 | 0.06917  | 0.74236  | -0.50608 |
| 3.08148  | -0.91224 | 1.10580  | 2.75213  | 0.54215  | -0.50952 | 0.01627  |
| $x_{22}$ | $x_{23}$ | $x_{24}$ | $x_{25}$ | $x_{26}$ | $x_{27}$ | $x_{28}$ |
| -1.24435 | -1.32192 | 1.67164  | 0.57368  | -0.85195 | 1.13292  | -0.13808 |
| 0.29925  | 0.18265  | 0.80070  | -1.49815 | -1.98915 | 1.68993  | 0.64309  |
| -0.18781 | 0.32869  | -0.45742 | 0.25999  | 2.56061  | -1.36947 | -1.09751 |

**Table 8.1.** Comparisons of ARL and SRL of  $MCD_n(0)$ ,  $LRC_n$ , SR, SA and SV (with  $k_u=1.5$ ,  $k_l=0.5$ ) charts for n=5, p=2,3, where  $\lambda=\lambda(\Sigma_o^{-1/2}\Sigma\Sigma_o^{-1/2})$ .

|        |      |          |              | p =                  | $= 2, \mu =$ | 0                    |              |                      |      |                      |
|--------|------|----------|--------------|----------------------|--------------|----------------------|--------------|----------------------|------|----------------------|
|        | MCI  | $D_5(0)$ | $\mathbf{S}$ | R                    | S            | A                    | $\mathbf{S}$ | V                    | LF   | RC                   |
|        | h=   | 4.3      | h=3          | 3.11                 | h =          | 16                   | h=3          | 3.66                 | h=1  | 18.6                 |
| λ      | ARL  | SRL      | ARL          | SRL                  | ARL          | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ |
| (1, 1) | 247  | 244      | 205          | 204                  | 203          | 202                  | 211          | 212                  | 248  | 241                  |
| $B_2$  | 26.1 | 21.3     | 55.1         | 55.0                 | 74.0         | 73.6                 | 651          | 565                  | 13.0 | 6.28                 |
| $C_2$  | 81.9 | 78.1     | 121          | 121                  | 153          | 153                  | 269          | 265                  | 45.2 | 27.5                 |
| $D_2$  | 20.0 | 16.9     | 31.8         | 30.9                 | 116          | 115                  | 41.5         | 40.8                 | 32.8 | 20.6                 |
| $E_2$  | 2.40 | 1.36     | 2.44         | 1.90                 | 4.35         | 3.78                 | 5.82         | 5.36                 | 3.17 | 1.84                 |
| $F_2$  | 17.8 | 14.9     | 27.5         | 26.6                 | 110          | 109                  | 32.9         | 32.2                 | 29.8 | 18.2                 |
| $G_2$  | 59.0 | 55.2     | 74.4         | 73.2                 | 181          | 181                  | 80.5         | 79.8                 | 102  | 73.7                 |
| $H_2$  | 93.9 | 90.2     | 119          | 117                  | 181          | 180                  | 158          | 158                  | 97.1 | 70.9                 |
| $J_2$  | 5.26 | 2.89     | 8.44         | 7.89                 | 5.41         | 4.87                 | >21          | .1                   | 2.57 | 0.91                 |
| $K_2$  | 2.32 | 1.25     | 2.21         | 1.64                 | 4.41         | 3.90                 | 2.56         | 2.04                 | 3.06 | 1.66                 |
|        |      |          |              | <i>p</i> =           | $= 3, \mu =$ | 0                    |              |                      |      |                      |
|        | MCI  | $D_5(0)$ | S            | R                    | S            | A                    | S            | V                    | LRC  |                      |
|        | h=4  | 4.95     | h=3          | 3.73                 | h=           | 28.7                 | h=4          | 4.05                 | h=2  | 29.8                 |
| λ      | ARL  | SRL      | ARL          | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ |
| (1, 1) | 209  | 206      | 206          | 206                  | 205          | 205                  | 197          | 196                  | 203  | 189                  |
| $B_3$  | 32.5 | 29.3     | 53.6         | 52.9                 | 181          | 181                  | 75.0         | 74.4                 | 78.3 | 51.6                 |
| $C_3$  | 35.9 | 32.4     | 58.6         | 58.0                 | 187          | 187                  | 69.0         | 68.2                 | 90.7 | 59.9                 |
| $D_3$  | 1.87 | 0.94     | 1.69         | 1.08                 | 4.81         | 4.31                 | 2.34         | 1.77                 | 2.80 | 1.44                 |
| $E_3$  | 12.4 | 0.60     | > 2          | 206                  | 12.9         | 12.6                 | > 1          | 197                  | 2.75 | 0.82                 |
| $F_3$  | 5.77 | 3.16     | 11.4         | 11.0                 | 11.5         | 10.9                 | >1           | 97                   | 3.06 | 1.07                 |
| $G_3$  | 24.1 | 17.7     | 62.7         | 62.4                 | 117          | 117                  | 423          | 409                  | 16.0 | 7.07                 |

**Table 8.2.** Comparisons of ARL and SRL of  $MCD_n(0)$ ,  $LRC_n$ , SR, SA and SV charts for n=5, p=2,3, where  $\lambda=\lambda(\Sigma_o^{-1/2}\Sigma\Sigma_o^{-1/2})$ .

|            |                  | p=2            | $\mu = 0$       |                   |                     |
|------------|------------------|----------------|-----------------|-------------------|---------------------|
|            | $MCD_5(0)$       | SR             | SA              | SV                | $LRC_5$             |
|            | h=2.34/0.72      | $h_u = 3.2$    | h=16.2          | h=3.66            | h=18.6              |
|            | $k_u = 1.5/0.72$ | $h_l = 0.493$  |                 |                   |                     |
|            | $k_l = 0.5/0.72$ |                |                 |                   |                     |
| λ          | ARL SRL          | ARL SRL        | ARL SRL         | ARL SRL           | ARL SRL             |
| (1.0, 1.0) | 247 244          | 219 209        | 219 219         | 211 211           | 248 240             |
| (0.2, 0.2) | $6.47 \ 0.57$    | 23.9  23.2     | $10.5 \ 10.0$   | >2000             | 2.91  0.91          |
| (0.4, 0.8) | $10.9 \ \ 2.83$  | 96.1 95.1      | 90.2 89.7       | >1981             | $11.0 \ \ 4.70$     |
| (0.8, 0.6) | $22.2 \ 11.5$    | $140 \ 139$    | 141 141         | > 1731            | 24.5 12.7           |
| (1.0, 0.6) | 24.2 13.3        | $156 \ 154$    | $153 \ 154$     | > 1269            | 28.8 15.1           |
| (1.6, 0.6) | 18.1 11.6        | 85.0 83.7      | $78.9 \ 78.3$   | $246 \ 244$       | 15.3 8.16           |
| (2.0, 0.6) | 11.2 8.04        | $36.2\ \ 35.6$ | $36.8 \ \ 36.4$ | 110 110           | 9.76  5.36          |
| (1.0, 0.8) | 99.9 88.3        | 199 193        | 201 198         | $506 	ext{ } 471$ | $93.3 \ 65.2$       |
| (1.4, 1.2) | $45.2 \ \ 43.9$  | 115 113        | 139 139         | $39.6 \ \ 38.7$   | 39.1  24.5          |
| (2.0, 1.2) | 11.0  9.79       | 30.0 29.6      | $42.7 \ 41.6$   | $16.5 \ 16.1$     | 12.3  7.19          |
| (1.6, 1.6) | 13.9  12.7       | $40.8 \ 40.3$  | 60.6 	 59.4     | $14.4 \ 14.0$     | 14.6 8.33           |
| (1.8, 1.6) | 10.5 9.22        | 29.1 28.4      | 44.5  43.6      | 11.4 11.0         | 11.6 - 6.63         |
| (2.0, 1.6) | 8.06 - 6.85      | $21.2 \ 20.9$  | $32.3 \ 31.6$   | $9.35 \ 8.97$     | 9.51  5.40          |
| (1.8, 1.8) | 8.29 7.18        | $22.4 \ 21.7$  | 33.9 33.1       | $9.16 \ 8.72$     | $9.69 	ext{ } 5.43$ |
| (2.0, 1.8) | 6.83  5.62       | $17.2 \ 16.8$  | 26.1  25.4      | 7.68  7.22        | 8.22 4.61           |
| (2.0, 2.0) | 5.74 4.62        | 13.8 13.5      | 20.9 20.2       | 6.49 6.01         | 7.16 4.00           |

Table 8.2. (continued)

|                 |            |          | 1            | $\rho = 3, \mu$ | = 0          |                      |              |                      |      |                      |
|-----------------|------------|----------|--------------|-----------------|--------------|----------------------|--------------|----------------------|------|----------------------|
|                 | MCI        | $D_5(0)$ | $\mathbf{S}$ | R               | $\mathbf{S}$ | A                    | $\mathbf{S}$ | V                    | LR   | $2C_5$               |
|                 | h = 2.3    | 34/0.75  | $h_u =$      | = 4.4           | h=28.7       |                      | h=4.05       |                      | h=2  | 29.8                 |
|                 | $k_u = 1$  | .5/0.75  | $h_l = 0$    | .49944          |              |                      |              |                      |      |                      |
|                 | $k_l = 0.$ | 5/0.75   |              |                 |              |                      |              |                      |      |                      |
| λ               | ARL        | SRL      | ARL          | SRL             | ARL          | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ |
| (1.0, 1.0, 1.0) | 209        | 206      | 213          | 205             | 205          | 205                  | 197          | 196                  | 203  | 189                  |
| (0.2, 0.2, 0.2) | 7.74       | 0.54     | 45.9         | 45.8            | 12.4         | 12.0                 | >2           | 000                  | 2.74 | 0.84                 |
| (0.2, 0.6, 1.4) | 8.19       | 1.19     | 83.8         | 83.5            | 52.6         | 52.5                 | >1           | 988                  | 5.77 | 1.93                 |
| (0.2, 1.4, 2.0) | 6.40       | 2.53     | 49.7         | 48.8            | 32.8         | 32.4                 | 893          | 673                  | 5.04 | 1.88                 |
| (0.4, 0.8, 0.8) | 12.3       | 2.68     | 132          | 132             | 115          | 115                  | >1           | 905                  | 13.1 | 5.15                 |
| (0.4, 0.8, 1.2) | 12.2       | 2.90     | 139          | 138             | 115          | 114                  | >1           | 560                  | 13.2 | 5.24                 |
| (0.6, 1.8, 2.0) | 7.29       | 5.29     | 43.1         | 42.2            | 50.2         | 49.3                 | 36.2         | 35.9                 | 9.02 | 4.38                 |
| (0.6, 2.0, 2.0) | 6.21       | 4.52     | 34.0         | 33.5            | 41.7         | 40.9                 | 29.7         | 28.7                 | 8.00 | 3.91                 |
| (0.8, 0.8, 2.0) | 12.9       | 10.9     | 78.1         | 76.3            | 82.7         | 82.0                 | 107          | 107                  | 15.0 | 7.89                 |
| (0.8, 1.0, 1.4) | 45.6       | 39.0     | 189          | 184             | 165          | 167                  | 147          | 147                  | 42.1 | 23.2                 |
| (1.2, 1.6, 1.8) | 9.81       | 8.40     | 64.1         | 63.3            | 89.9         | 89.7                 | 16.5         | 15.9                 | 16.2 | 8.53                 |
| (1.2, 1.8, 2.0) | 6.60       | 5.39     | 37.2         | 36.5            | 59.6         | 59.0                 | 12.3         | 11.8                 | 11.4 | 5.97                 |
| (1.4, 1.8, 1.8) | 7.39       | 6.08     | 44.1         | 43.4            | 71.0         | 70.3                 | 11.3         | 10.7                 | 12.8 | 6.72                 |
| (1.6, 1.6, 1.6) | 9.51       | 8.24     | 63.2         | 62.6            | 94.3         | 92.5                 | 13.1         | 12.6                 | 16.7 | 8.73                 |
| (1.6, 1.8, 2.0) | 5.68       | 4.43     | 29.6         | 28.9            | 53.0         | 52.8                 | 8.46         | 7.96                 | 10.1 | 5.24                 |
| (1.8, 1.8, 2.0) | 5.16       | 3.95     | 25.5         | 25.2            | 47.1         | 47.0                 | 7.38         | 6.88                 | 9.29 | 4.75                 |
| (1.8, 2.0, 2.0) | 4.61       | 3.41     | 21.1         | 20.8            | 39.8         | 39.0                 | 6.54         | 6.04                 | 8.28 | 4.21                 |

**Table 9.1.** The out-of-control ARL and SRL of  $MCD_2(0)$  with  $p = 3, \mu = 0, h = 10/0.74, <math>k_u = 1.5/0.74, k_l = 0.5/0.74$  and the in-control (ARL,SRL)= (170, 161) where  $\lambda = \lambda(\Sigma_o^{-1/2}\Sigma\Sigma_o^{-1/2})$ .

| λ               | ARL  | SRL  | λ               | ARL  | SRL  | λ               | ARL  | SRL  |
|-----------------|------|------|-----------------|------|------|-----------------|------|------|
| (0.2, 0.2, 0.2) | 24.9 | 1.49 | (0.2, 0.8, 1.4) | 26.0 | 5.89 | (0.4, 0.4, 1.4) | 33.4 | 9.44 |
| (0.2, 0.4, 0.6) | 27.3 | 2.58 | (0.2, 1.2, 1.4) | 24.7 | 7.05 | (0.4, 0.6, 2.0) | 25.7 | 14.4 |
| (0.2, 0.4, 1.4) | 26.1 | 5.18 | (0.2, 1.4, 1.4) | 23.4 | 7.95 | (0.4, 0.8, 1.4) | 37.7 | 14.0 |
| (0.2, 0.4, 2.0) | 21.2 | 8.42 | (0.2, 1.4, 2.0) | 18.0 | 9.32 | (0.4, 0.8, 2.0) | 25.4 | 14.8 |
| (0.2, 0.6, 0.6) | 27.6 | 2.80 | (0.2, 1.6, 1.6) | 20.1 | 9.06 | (0.4, 1.0, 1.0) | 41.7 | 12.3 |
| (0.2, 0.6, 1.6) | 24.7 | 6.94 | (0.2, 2.0, 2.0) | 13.9 | 8.81 | (0.4, 1.0, 2.0) | 24.4 | 14.9 |
| (0.2, 0.6, 2.0) | 21.0 | 8.67 | (0.4, 0.4, 0.6) | 35.0 | 6.14 | (0.4, 1.2, 1.4) | 34.7 | 15.3 |
| (0.2, 0.8, 0.8) | 27.7 | 3.03 | (0.4, 0.4, 0.8) | 35.7 | 6.48 | (0.4, 1.2, 1.6) | 30.6 | 15.7 |
| (0.2, 0.8, 1.2) | 27.1 | 4.34 | (0.4, 0.4, 1.2) | 35.1 | 7.92 | (0.4, 1.2, 2.0) | 22.9 | 14.6 |
| (0.6, 0.6, 0.8) | 59.2 | 22.9 | (0.6, 1.6, 2.0) | 19.6 | 16.0 | (0.8, 2.0, 2.0) | 14.2 | 11.9 |
| (0.6, 0.6, 1.6) | 43.7 | 25.1 | (0.8, 0.8, 0.8) | 126  | 87.0 | (1.0, 1.0, 1.8) | 34.1 | 31.0 |
| (0.6, 0.6, 1.8) | 35.8 | 22.6 | (0.8, 0.8, 1.0) | 146  | 111  | (1.0, 1.0, 2.0) | 26.0 | 22.9 |
| (0.6, 0.8, 1.0) | 78.0 | 42.2 | (0.8.0.8, 1.6)  | 57.2 | 47.8 | (1.0, 1.2, 1.6) | 40.0 | 37.7 |
| (0.6, 0.8, 1.4) | 60.6 | 37.9 | (0.8, 0.8, 2.0) | 30.2 | 25.6 | (1.0, 1.2, 2.0) | 23.3 | 20.6 |
| (0.6, 1.0, 2.0) | 28.0 | 21.7 | (0.8, 1.2, 1.6) | 44.6 | 40.3 | (1.0, 1.8, 2.0) | 15.3 | 13.0 |
| (1.6, 1.6, 1.8) | 14.8 | 12.5 | (1.2, 1.2, 1.4) | 45.3 | 42.3 | (1.6, 1.6, 2.0) | 13.0 | 10.7 |
| (1.2, 1.2, 1.6) | 33.7 | 30.9 | (1.6, 1.8, 1.8) | 13.1 | 11.0 | (1.2, 1.2, 1.8) | 26.1 | 23.2 |
| (1.8, 1.8, 2.0) | 10.7 | 8.61 | (1.2, 1.4, 1.8) | 22.6 | 20.0 | (1.8, 2.0, 2.0) | 9.76 | 7.75 |
| (1.4, 1.4, 1.6) | 23.7 | 21.2 | (1.4, 1.4, 1.8) | 19.5 | 16.9 | (1.4, 1.4, 2.0) | 16.4 | 13.9 |

**Extended Table 8.2.** Comparisons of ARL and SRL of  $MCD_n(0)$ ,  $LRC_n$ , SR, SA and SV charts for n=5, p=2,3, where  $\lambda=\lambda(\Sigma_o^{-1/2}\Sigma\Sigma_o^{-1/2})$ .

|            |            |          |         | p=2   | $\mu = 0$    |      |       |      |      |        |
|------------|------------|----------|---------|-------|--------------|------|-------|------|------|--------|
|            | MCI        | $D_5(0)$ | S       | R     | $\mathbf{S}$ | A    | S     | V    | LR   | $2C_5$ |
|            | h=2.3      | 4/0.72   | $h_u$ = | =3.2  | h=1          | 16.2 | h=3   | 3.66 | h=1  | 18.6   |
|            | $k_u = 1$  | .5/0.72  | $h_l =$ | 0.493 |              |      |       |      |      |        |
|            | $k_l = 0.$ | 5/0.72   |         |       |              |      |       |      |      |        |
| λ          | ARL        | SRL      | ARL     | SRL   | ARL          | SRL  | ARL   | SRL  | ARL  | SRL    |
| (1.0, 1.0) | 247        | 244      | 219     | 209   | 219          | 219  | 211   | 211  | 248  | 240    |
| (0.2, 0.2) | 6.47       | 0.57     | 23.9    | 23.2  | 10.5         | 10.0 | >20   | 000  | 2.91 | 0.91   |
| (0.2, 0.4) | 6.87       | 0.74     | 35.2    | 34.6  | 21.6         | 20.9 | >20   | 000  | 3.94 | 1.33   |
| (0.2, 0.6) | 6.95       | 0.78     | 40.8    | 40.1  | 31.4         | 30.9 | >20   | 000  | 4.67 | 1.60   |
| (0.2, 0.8) | 6.97       | 0.79     | 43.9    | 43.1  | 38.7         | 38.0 | >20   | 000  | 5.08 | 1.72   |
| (0.2, 1.0) | 6.97       | 0.82     | 45.7    | 45.2  | 41.2         | 40.7 | >20   | 000  | 5.20 | 1.75   |
| (0.2, 1.2) | 6.94       | 0.91     | 45.9    | 45.3  | 38.9         | 38.0 | >20   | 000  | 5.12 | 1.73   |
| (0.2, 1.4) | 6.84       | 1.09     | 43.6    | 43.0  | 32.9         | 32.3 | >19   | 993  | 4.91 | 1.71   |
| (0.2, 1.6) | 6.62       | 1.36     | 38.7    | 38.1  | 25.8         | 25.7 | >1981 |      | 4.65 | 1.66   |
| (0.2, 1.8) | 6.32       | 1.63     | 31.7    | 30.8  | 20.0         | 19.8 | >19   | 957  | 4.37 | 1.60   |
| (0.2, 2.0) | 5.94       | 1.87     | 25.1    | 24.5  | 15.5         | 15.2 | >19   | 911  | 4.09 | 1.58   |
| (0.4, 0.4) | 9.12       | 1.73     | 64.1    | 63.7  | 47.8         | 47.4 | >20   | 000  | 6.44 | 2.50   |
| (0.4, 0.6) | 10.5       | 2.56     | 83.3    | 82.7  | 71.8         | 71.0 | >20   | 000  | 9.01 | 3.80   |
| (0.4, 0.8) | 10.9       | 2.83     | 96.1    | 95.1  | 90.2         | 89.7 | >19   | 981  | 11.0 | 4.70   |
| (0.4, 1.0) | 11.0       | 2.97     | 104     | 103   | 97.3         | 96.7 | >19   | 911  | 11.8 | 4.96   |
| (0.4, 1.2) | 10.9       | 3.10     | 103     | 103   | 90.6         | 90.0 | >1'   | 731  | 11.3 | 4.81   |
| (0.4, 1.4) | 10.6       | 3.25     | 90.2    | 89.4  | 73.6         | 73.9 | > 1   | 449  | 10.2 | 4.44   |
| (0.4, 1.6) | 9.96       | 3.51     | 69.5    | 68.9  | 53.9         | 53.7 | > 1   | 086  | 8.94 | 4.00   |
| (0.4, 1.8) | 9.12       | 3.74     | 49.1    | 48.3  | 38.4         | 38.1 | 753   | 619  | 7.80 | 3.62   |
| (0.4, 2.0) | 8.11       | 3.84     | 34.1    | 33.5  | 27.7         | 27.5 | 506   | 471  | 6.85 | 3.25   |
| (0.6, 0.6) | 16.5       | 6.63     | 116     | 116   | 112          | 112  | >19   | 957  | 15.9 | 7.70   |
| (0.8, 0.6) | 22.2       | 11.5     | 140     | 139   | 141          | 141  | > 1   | 731  | 24.5 | 12.7   |
| (1.0, 0.6) | 24.2       | 13.3     | 156     | 154   | 153          | 154  | > 1   | 269  | 28.8 | 15.1   |
| (1.2, 0.6) | 23.9       | 13.7     | 152     | 150   | 142          | 142  | 753   | 619  | 25.6 | 13.5   |
| (1.4, 0.6) | 21.8       | 13.0     | 124     | 122   | 112          | 111  | 416   | 398  | 20.0 | 10.6   |

Extended Table 8.2. (continued)

|            |      |                      |              | p =                  | $2, \mu = 0$ | (0011011             |              |                      |      |        |
|------------|------|----------------------|--------------|----------------------|--------------|----------------------|--------------|----------------------|------|--------|
|            | MCI  | $D_5(0)$             | $\mathbf{S}$ | R                    | $\mathbf{S}$ | A                    | $\mathbf{S}$ | V                    | LR   | $2C_5$ |
| λ          | ARL  | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL  | SRL    |
| (1.6, 0.6) | 18.1 | 11.6                 | 85.0         | 83.7                 | 78.9         | 78.3                 | 246          | 244                  | 15.3 | 8.16   |
| (1.8, 0.6) | 14.3 | 9.73                 | 55.3         | 54.9                 | 53.9         | 53.3                 | 158          | 158                  | 12.0 | 6.51   |
| (2.0, 0.6) | 11.2 | 8.04                 | 36.2         | 35.6                 | 36.8         | 36.4                 | 110          | 110                  | 9.76 | 5.36   |
| (0.8, 0.8) | 59.3 | 47.5                 | 178          | 174                  | 182          | 182                  | >1           | 086                  | 56.6 | 35.3   |
| (1.0, 0.8) | 99.9 | 88.3                 | 199          | 193                  | 201          | 198                  | 506          | 471                  | 93.3 | 65.2   |
| (1.2, 0.8) | 87.7 | 79.0                 | 187          | 182                  | 183          | 180                  | 246          | 244                  | 64.1 | 41.5   |
| (1.4, 0.8) | 53.6 | 48.3                 | 139          | 137                  | 140          | 139                  | 139          | 138                  | 35.9 | 22.1   |
| (1.6, 0.8) | 30.6 | 27.3                 | 89.2         | 87.7                 | 96.3         | 95.4                 | 88.9         | 88.6                 | 22.6 | 13.6   |
| (1.8, 0.8) | 18.8 | 16.7                 | 55.6         | 55.1                 | 63.4         | 62.8                 | 61.5         | 61.2                 | 15.8 | 9.39   |
| (2.0, 0.8) | 12.7 | 11.1                 | 35.7         | 35.0                 | 42.5         | 41.8                 | 45.4         | 45.1                 | 12.0 | 7.06   |
| (1.2, 1.0) | 138  | 136                  | 196          | 189                  | 200          | 199                  | 110          | 110                  | 117  | 88     |
| (1.4, 1.0) | 61.0 | 60.3                 | 137          | 135                  | 151          | 149                  | 66.7         | 66.8                 | 47.2 | 30.6   |
| (1.6, 1.0) | 30.7 | 29.2                 | 84.3         | 82.7                 | 103          | 102                  | 45.4         | 45.1                 | 26.2 | 16.4   |
| (1.8, 1.0) | 18.2 | 16.7                 | 52.2         | 51.4                 | 66.8         | 65.7                 | 32.9         | 32.2                 | 17.4 | 10.5   |
| (2.0, 1.0) | 12.2 | 10.9                 | 33.6         | 32.7                 | 44.2         | 43.3                 | 25.4         | 24.7                 | 12.8 | 7.69   |
| (1.2, 1.2) | 85.1 | 83.8                 | 167          | 164                  | 182          | 182                  | 61.5         | 61.2                 | 74.6 | 50.3   |
| (1.4, 1.2) | 45.2 | 43.9                 | 115          | 113                  | 139          | 139                  | 39.6         | 38.7                 | 39.1 | 24.5   |
| (1.6, 1.2) | 24.9 | 23.7                 | 71.6         | 70.8                 | 96.2         | 95.7                 | 27.9         | 27.2                 | 23.6 | 14.4   |
| (1.8, 1.2) | 15.9 | 14.6                 | 45.5         | 44.3                 | 63.9         | 62.7                 | 21.0         | 20.4                 | 16.3 | 9.65   |
| (2.0, 1.2) | 11.0 | 9.79                 | 30.0         | 29.6                 | 42.7         | 41.6                 | 16.5         | 16.1                 | 12.3 | 7.19   |
| (1.4, 1.4) | 29.2 | 27.9                 | 82.3         | 81.9                 | 112          | 111                  | 26.6         | 25.9                 | 26.8 | 16.2   |
| (1.6, 1.4) | 18.9 | 18.0                 | 55.7         | 54.8                 | 79.5         | 78.4                 | 19.2         | 18.6                 | 18.7 | 11.1   |
| (1.8, 1.4) | 13.1 | 11.9                 | 37.2         | 36.2                 | 55.1         | 53.8                 | 14.9         | 14.6                 | 13.9 | 8.00   |
| (2.0, 1.4) | 9.52 | 8.38                 | 25.7         | 25.3                 | 38.2         | 37.6                 | 12.0         | 11.6                 | 10.9 | 6.29   |
| (1.6, 1.6) | 13.9 | 12.7                 | 40.8         | 40.3                 | 60.6         | 59.4                 | 14.4         | 14.0                 | 14.6 | 8.33   |
| (1.8, 1.6) | 10.5 | 9.22                 | 29.1         | 28.4                 | 44.5         | 43.6                 | 11.4         | 11.0                 | 11.6 | 6.63   |
| (2.0, 1.6) | 8.06 | 6.85                 | 21.2         | 20.9                 | 32.3         | 31.6                 | 9.35         | 8.97                 | 9.51 | 5.40   |
| (1.8, 1.8) | 8.29 | 7.18                 | 22.4         | 21.7                 | 33.9         | 33.1                 | 9.16         | 8.72                 | 9.69 | 5.43   |
| (2.0, 1.8) | 6.83 | 5.62                 | 17.2         | 16.8                 | 26.1         | 25.4                 | 7.68         | 7.22                 | 8.22 | 4.61   |
| (2.0, 2.0) | 5.74 | 4.62                 | 13.8         | 13.5                 | 20.9         | 20.2                 | 6.49         | 6.01                 | 7.16 | 4.00   |

Extended Table 8.2. (continued)

|                 |            |                      | 1         | $\rho = 3, \mu$      | = 0  |                      |                  |      |      |                      |
|-----------------|------------|----------------------|-----------|----------------------|------|----------------------|------------------|------|------|----------------------|
|                 | MCI        | $D_5(0)$             | S         | R                    | S    | A                    | $\mathbf{S}^{-}$ | V    | LR   | $2C_5$               |
|                 | h = 2.3    | 34/0.75              | $h_u =$   | = 4.4                | h=   | 28.7                 | h=4              | 4.05 | h=2  | 29.8                 |
|                 | $k_u = 1$  | .5/0.75              | $h_l = 0$ | .49944               |      |                      |                  |      |      |                      |
|                 | $k_l = 0.$ | .5/0.75              |           |                      |      |                      |                  |      |      |                      |
| λ               | ARL        | $\operatorname{SRL}$ | ARL       | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ | ARL              | SRL  | ARL  | $\operatorname{SRL}$ |
| (1.0, 1.0, 1.0) | 209        | 206                  | 213       | 205                  | 205  | 205                  | 197              | 196  | 203  | 189                  |
| (0.2, 0.2, 0.2) | 7.74       | 0.54                 | 45.9      | 45.8                 | 12.4 | 12.0                 | >20              | 000  | 2.74 | 0.84                 |
| (0.2, 0.2, 0.4) | 7.94       | 0.58                 | 54.5      | 54.0                 | 19.4 | 19.3                 | >20              | 000  | 3.30 | 1.03                 |
| (0.2, 0.2, 0.6) | 7.96       | 0.58                 | 58.2      | 57.4                 | 24.4 | 24.3                 | >20              | 000  | 3.63 | 1.12                 |
| (0.2, 0.2, 0.8) | 7.98       | 0.59                 | 59.9      | 59.3                 | 26.8 | 26.5                 | >20              | 000  | 3.77 | 1.16                 |
| (0.2, 0.2, 1.0) | 7.98       | 0.60                 | 60.3      | 60.0                 | 27.9 | 27.7                 | >20              | 000  | 3.81 | 1.18                 |
| (0.2, 0.2, 1.2) | 7.95       | 0.70                 | 60.8      | 60.5                 | 27.1 | 27.0                 | >20              | 000  | 3.79 | 1.18                 |
| (0.2, 0.2, 1.4) | 7.86       | 0.95                 | 60.5      | 60.4                 | 25.2 | 24.9                 | >20              | 000  | 3.71 | 1.16                 |
| (0.2, 0.2, 1.6) | 7.63       | 1.34                 | 59.0      | 58.1                 | 22.4 | 22.0                 | >20              | 000  | 3.61 | 1.15                 |
| (0.2, 0.2, 1.8) | 7.31       | 1.67                 | 53.8      | 53.6                 | 19.6 | 18.9                 | >20              | 000  | 3.49 | 1.14                 |
| (0.2, 0.2, 2.0) | 6.82       | 2.05                 | 47.1      | 46.0                 | 16.8 | 16.6                 | >20              | 000  | 3.36 | 1.13                 |
| (0.2, 0.4, 0.4) | 8.26       | 0.71                 | 65.3      | 64.9                 | 31.8 | 31.4                 | >20              | 000  | 4.21 | 1.35                 |
| (0.2, 0.4, 0.6) | 8.30       | 0.76                 | 71.8      | 70.9                 | 40.6 | 40.3                 | >20              | 000  | 4.77 | 1.57                 |
| (0.2, 0.4, 0.8) | 8.32       | 0.74                 | 74.7      | 73.6                 | 45.1 | 44.3                 | >20              | 000  | 5.05 | 1.69                 |
| (0.2, 0.4, 1.0) | 8.32       | 0.77                 | 75.6      | 75.8                 | 46.6 | 45.9                 | >20              | 000  | 5.16 | 1.67                 |
| (0.2, 0.4, 1.2) | 8.29       | 0.87                 | 77.5      | 76.6                 | 45.7 | 44.9                 | >20              | 000  | 5.10 | 1.65                 |
| (0.2, 0.4, 1.4) | 8.18       | 1.11                 | 76.7      | 75.9                 | 45.7 | 44.9                 | >20              | 000  | 4.96 | 1.63                 |
| (0.2, 0.4, 1.6) | 7.95       | 1.47                 | 71.8      | 72.4                 | 37.0 | 36.4                 | >19              | 997  | 4.73 | 1.61                 |
| (0.2, 0.4, 1.8) | 7.54       | 1.88                 | 65.2      | 64.0                 | 30.9 | 30.6                 | >19              | 995  | 4.53 | 1.56                 |
| (0.2, 0.4, 2.0) | 7.00       | 2.21                 | 54.9      | 53.8                 | 25.7 | 25.3                 | >19              | 989  | 4.29 | 1.53                 |
| (0.2, 0.6, 0.6) | 8.35       | 0.76                 | 78.1      | 76.8                 | 51.0 | 50.3                 | >20              | 000  | 5.53 | 1.85                 |
| (0.2, 0.6, 0.8) | 8.37       | 0.77                 | 81.4      | 80.8                 | 58.1 | 57.6                 | >20              | 000  | 5.94 | 1.96                 |
| (0.2, 0.6, 1.0) | 8.37       | 0.79                 | 83.8      | 83.4                 | 60.2 | 59.9                 | >19              | 998  | 6.09 | 1.98                 |
| (0.2, 0.6, 1.2) | 8.34       | 0.90                 | 84.9      | 84.7                 | 58.1 | 57.8                 | >19              | 995  | 5.98 | 1.98                 |
| (0.2, 0.6, 1.4) | 8.19       | 1.19                 | 83.8      | 83.5                 | 52.6 | 52.5                 | >19              | 988  | 5.77 | 1.93                 |

Extended Table 8.2. (continued)

|                 |      |                      |      | p=3, | $\mu = 0$ |                      |     |     |      |        |
|-----------------|------|----------------------|------|------|-----------|----------------------|-----|-----|------|--------|
|                 | MCI  | $D_5(0)$             | S    | R    | S         | A                    | S   | V   | LR   | $2C_5$ |
| λ               | ARL  | $\operatorname{SRL}$ | ARL  | SRL  | ARL       | $\operatorname{SRL}$ | ARL | SRL | ARL  | SRL    |
| (0.2, 0.6, 1.6) | 7.95 | 1.54                 | 78.7 | 77.5 | 46.5      | 46.2                 | >19 | 974 | 5.48 | 1.88   |
| (0.2, 0.6, 1.8) | 7.52 | 1.95                 | 68.6 | 68.8 | 38.6      | 38.5                 | >19 | 952 | 5.16 | 1.82   |
| (0.2, 0.6, 2.0) | 6.97 | 2.28                 | 56.4 | 55.0 | 31.9      | 31.9                 | >19 | 927 | 4.91 | 1.78   |
| (0.2, 0.8, 0.8) | 8.38 | 0.78                 | 85.4 | 85.1 | 65.7      | 65.2                 | >19 | 997 | 6.44 | 2.11   |
| (0.2, 0.8, 1.0) | 8.37 | 0.81                 | 87.4 | 87.7 | 67.0      | 67.0                 | >19 | 990 | 6.61 | 2.12   |
| (0.2, 0.8, 1.2) | 8.34 | 0.93                 | 88.3 | 88.8 | 65.5      | 65.5                 | >19 | 974 | 6.46 | 2.13   |
| (0.2, 0.8, 1.4) | 8.18 | 1.25                 | 86.8 | 87.3 | 59.8      | 59.2                 | >19 | 944 | 6.21 | 2.08   |
| (0.2, 0.8, 1.6) | 7.92 | 1.59                 | 81.1 | 80.2 | 51.2      | 50.8                 | >19 | 907 | 5.88 | 2.03   |
| (0.2, 0.8, 1.8) | 7.47 | 1.99                 | 70.6 | 69.3 | 42.8      | 42.5                 | >18 | 848 | 5.53 | 1.95   |
| (0.2, 0.8, 2.0) | 6.91 | 2.33                 | 57.4 | 56.0 | 35.2      | 34.9                 | >1' | 767 | 5.17 | 1.91   |
| (0.2, 1.0, 1.0) | 8.37 | 0.88                 | 90.3 | 90.4 | 70.4      | 70.3                 | >19 | 970 | 6.77 | 2.16   |
| (0.2, 1.0, 1.2) | 8.31 | 1.04                 | 91.1 | 91.1 | 68.5      | 67.5                 | >19 | 929 | 6.67 | 2.15   |
| (0.2, 1.0, 1.4) | 8.15 | 1.31                 | 88.9 | 89.3 | 61.9      | 61.3                 | >18 | 866 | 6.36 | 2.10   |
| (0.2, 1.0, 1.6) | 7.85 | 1.66                 | 81.3 | 81.1 | 53.6      | 52.9                 | >1' | 765 | 6.05 | 2.06   |
| (0.2, 1.0, 1.8) | 7.36 | 2.09                 | 69.5 | 69.0 | 44.4      | 44.2                 | >10 | 646 | 5.62 | 2.00   |
| (0.2, 1.0, 2.0) | 6.84 | 2.35                 | 56.0 | 54.8 | 36.1      | 35.7                 | >1  | 497 | 5.25 | 1.95   |
| (0.2, 1.2, 1.2) | 8.22 | 1.23                 | 91.3 | 91.3 | 65.0      | 64.6                 | >18 | 848 | 6.53 | 2.14   |
| (0.2, 1.2, 1.4) | 8.03 | 1.49                 | 88.2 | 88.2 | 60.0      | 59.3                 | >1' | 719 | 6.27 | 2.08   |
| (0.2, 1.2, 1.6) | 7.72 | 1.82                 | 80.1 | 78.8 | 51.7      | 51.3                 | >1  | 559 | 5.92 | 2.04   |
| (0.2, 1.2, 1.8) | 7.24 | 2.18                 | 67.0 | 66.3 | 43.0      | 42.6                 | >13 | 379 | 5.57 | 1.97   |
| (0.2, 1.2, 2.0) | 6.64 | 2.45                 | 53.5 | 52.5 | 35.2      | 34.7                 | >1  | 184 | 5.24 | 1.93   |
| (0.2, 1.4, 1.4) | 7.82 | 1.73                 | 83.2 | 83.2 | 54.9      | 54.0                 | >1  | 532 | 6.04 | 2.04   |
| (0.2, 1.4, 1.6) | 7.44 | 2.08                 | 75.0 | 73.7 | 47.4      | 47.4                 | >13 | 312 | 5.74 | 1.99   |
| (0.2, 1.4, 1.8) | 6.98 | 2.31                 | 62.2 | 60.8 | 39.9      | 39.4                 | >10 | 094 | 5.37 | 1.94   |
| (0.2, 1.4, 2.0) | 6.40 | 2.53                 | 49.7 | 48.8 | 32.8      | 32.4                 | 893 | 673 | 5.04 | 1.88   |

Extended Table 8.2. (continued)

|                 |      |                      |      | p=3,                 | $\mu = 0$ |                      |              |     |      |        |
|-----------------|------|----------------------|------|----------------------|-----------|----------------------|--------------|-----|------|--------|
|                 | MCI  | $D_5(0)$             | S    | R                    | S         | A                    | $\mathbf{S}$ | V   | LR   | $2C_5$ |
| λ               | ARL  | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ | ARL       | $\operatorname{SRL}$ | ARL          | SRL | ARL  | SRL    |
| (0.2, 1.6, 1.6) | 7.07 | 2.30                 | 66.6 | 65.4                 | 41.8      | 41.7                 | >1           | 065 | 5.45 | 1.93   |
| (0.2, 1.6, 1.8) | 6.62 | 2.44                 | 55.1 | 54.2                 | 35.3      | 34.8                 | 840          | 656 | 5.13 | 1.88   |
| (0.2, 1.6, 2.0) | 6.09 | 2.58                 | 44.0 | 43.4                 | 29.5      | 28.5                 | 649          | 566 | 4.86 | 1.82   |
| (0.2, 1.8, 1.8) | 6.21 | 2.56                 | 46.4 | 46.0                 | 30.6      | 29.9                 | 629          | 554 | 4.89 | 1.84   |
| (0.2, 1.8, 2.0) | 5.73 | 2.61                 | 37.1 | 36.3                 | 25.6      | 24.6                 | 476          | 447 | 4.62 | 1.76   |
| (0.2, 2.0, 2.0) | 5.30 | 2.60                 | 30.7 | 30.2                 | 21.9      | 20.9                 | 356          | 346 | 4.39 | 1.70   |
| (0.4, 0.4, 0.4) | 10.3 | 1.48                 | 90.8 | 89.1                 | 54.5      | 54.2                 | >2           | 000 | 6.04 | 2.15   |
| (0.4, 0.4, 0.6) | 10.9 | 1.77                 | 101  | 99.2                 | 69.6      | 70.3                 | >2           | 000 | 7.37 | 2.67   |
| (0.4, 0.4, 0.8) | 11.0 | 1.81                 | 107  | 106                  | 79.0      | 78.9                 | >1           | 998 | 8.19 | 3.02   |
| (0.4, 0.4, 1.0) | 11.1 | 1.90                 | 111  | 111                  | 82.3      | 82.2                 | >1           | 989 | 8.43 | 3.12   |
| (0.4, 0.4, 1.2) | 11.0 | 2.00                 | 112  | 112                  | 78.8      | 78.0                 | >1           | 974 | 8.23 | 3.02   |
| (0.4, 0.4, 1.4) | 10.8 | 2.31                 | 111  | 111                  | 72.0      | 71.7                 | >1           | 944 | 7.79 | 2.88   |
| (0.4, 0.4, 1.6) | 10.3 | 2.70                 | 101  | 101                  | 61.9      | 61.8                 | >1           | 906 | 7.30 | 2.77   |
| (0.4, 0.4, 1.8) | 9.49 | 3.11                 | 87.6 | 86.3                 | 51.8      | 51.3                 | >1           | 848 | 6.69 | 2.62   |
| (0.4, 0.4, 2.0) | 8.59 | 3.40                 | 69.2 | 67.3                 | 42.0      | 41.1                 | >1           | 767 | 6.16 | 2.48   |
| (0.4, 0.6, 0.6) | 11.8 | 2.28                 | 114  | 114                  | 89.9      | 90.3                 | >1           | 995 | 9.60 | 3.68   |
| (0.4, 0.6, 0.8) | 12.0 | 2.50                 | 121  | 121                  | 101       | 101                  | >1           | 976 | 11.1 | 4.27   |
| (0.4, 0.6, 1.0) | 12.1 | 2.58                 | 127  | 127                  | 104       | 104                  | >1           | 929 | 11.5 | 4.49   |
| (0.4, 0.6, 1.2) | 12.0 | 2.72                 | 128  | 128                  | 101       | 101                  | >1           | 849 | 11.2 | 4.33   |
| (0.4, 0.6, 1.4) | 11.7 | 3.01                 | 126  | 126                  | 91.8      | 91.8                 | >1           | 559 | 10.4 | 4.07   |
| (0.4, 0.6, 1.6) | 11.0 | 3.40                 | 114  | 114                  | 78.9      | 78.9                 | >1           | 559 | 9.39 | 3.77   |
| (0.4, 0.6, 1.8) | 10.1 | 3.76                 | 94.3 | 94.2                 | 64.9      | 65.3                 | >1           | 379 | 8.40 | 3.50   |
| (0.4, 0.6, 2.0) | 8.95 | 3.96                 | 72.9 | 71.7                 | 51.7      | 51.1                 | >1           | 184 | 7.57 | 3.20   |
| (0.4, 0.8, 0.8) | 12.3 | 2.68                 | 132  | 132                  | 115       | 115                  | >1           | 905 | 13.1 | 5.15   |
| (0.4, 0.8, 1.0) | 12.3 | 2.76                 | 137  | 138                  | 119       | 119                  | >1           | 767 | 13.7 | 5.42   |
| (0.4, 0.8, 1.2) | 12.2 | 2.90                 | 139  | 138                  | 115       | 114                  | >1           | 560 | 13.2 | 5.24   |

Extended Table 8.2. (continued)

|                 |      |                      |              | p=3,                 | $\mu = 0$    |                      |              |      |      |        |
|-----------------|------|----------------------|--------------|----------------------|--------------|----------------------|--------------|------|------|--------|
|                 | MCI  | $D_5(0)$             | $\mathbf{S}$ | R                    | $\mathbf{S}$ | A                    | $\mathbf{S}$ | V    | LF   | $2C_5$ |
| λ               | ARL  | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL          | SRL  | ARL  | SRL    |
| (0.4, 0.8, 1.4) | 11.9 | 3.20                 | 135          | 135                  | 104          | 104                  | >1           | 316  | 12.1 | 4.87   |
| (0.4, 0.8, 1.6) | 11.1 | 3.72                 | 120          | 120                  | 88.6         | 88.6                 | >1           | 065  | 10.8 | 4.40   |
| (0.4, 0.8, 1.8) | 10.1 | 4.01                 | 96.3         | 95.6                 | 72.3         | 72.4                 | 840          | 656  | 9.50 | 3.40   |
| (0.4, 0.8, 2.0) | 8.88 | 4.14                 | 73.1         | 71.6                 | 57.0         | 55.9                 | 649          | 566  | 8.41 | 3.66   |
| (0.4, 1.0, 1.0) | 12.4 | 2.86                 | 142          | 140                  | 124          | 124                  | >1           | 497  | 14.5 | 5.64   |
| (0.4, 1.0, 1.2) | 12.3 | 3.04                 | 145          | 145                  | 119          | 120                  | >1           | 185  | 13.9 | 5.50   |
| (0.4, 1.0, 1.4) | 11.8 | 3.38                 | 139          | 139                  | 108          | 109                  | 892          | 673  | 12.6 | 5.10   |
| (0.4, 1.0, 1.6) | 11.0 | 3.74                 | 121          | 120                  | 91.8         | 91.6                 | 649          | 566  | 11.3 | 4.59   |
| (0.4, 1.0, 1.8) | 9.92 | 4.07                 | 94.8         | 93.5                 | 74.5         | 74.0                 | 476          | 447  | 9.92 | 4.24   |
| (0.4, 1.0, 2.0) | 8.73 | 4.13                 | 69.6         | 68.1                 | 59.1         | 58.3                 | 356          | 346  | 8.73 | 3.85   |
| (0.4, 1.2, 1.2) | 12.0 | 3.26                 | 144          | 143                  | 114          | 114                  | 839          | 660  | 13.4 | 5.33   |
| (0.4, 1.2, 1.4) | 11.5 | 3.55                 | 136          | 136                  | 105          | 105                  | 572          | 517  | 12.2 | 4.90   |
| (0.4, 1.2, 1.6) | 10.7 | 3.92                 | 116          | 115                  | 89.6         | 89.3                 | 398          | 384  | 10.9 | 4.47   |
| (0.4, 1.2, 1.8) | 9.60 | 4.17                 | 89.8         | 88.6                 | 89.6         | 89.3                 | 293          | 288  | 9.61 | 4.07   |
| (0.4, 1.2, 2.0) | 8.43 | 4.16                 | 65.5         | 64.3                 | 57.3         | 56.2                 | 220          | 220  | 5.01 | 1.66   |
| (0.4, 1.4, 1.4) | 11.0 | 3.82                 | 126          | 126                  | 95.6         | 95.9                 | 376          | 366  | 11.4 | 4.55   |
| (0.4, 1.4, 1.6) | 10.1 | 4.17                 | 105          | 104                  | 82.1         | 81.6                 | 262          | 259  | 10.2 | 4.24   |
| (0.4, 1.4, 1.8) | 9.04 | 4.23                 | 80.9         | 79.9                 | 67.2         | 65.8                 | 193          | 192  | 9.04 | 3.82   |
| (0.4, 1.4, 2.0) | 7.90 | 4.16                 | 59.2         | 58.8                 | 53.5         | 52.4                 | 147          | 147  | 8.12 | 3.57   |
| (0.4, 1.6, 1.6) | 9.33 | 4.24                 | 87.6         | 87.0                 | 70.2         | 70.0                 | 185          | 184  | 9.25 | 3.88   |
| (0.4, 1.6, 1.8) | 8.34 | 4.20                 | 67.9         | 67.1                 | 58.2         | 57.7                 | 139          | 137  | 8.32 | 3.56   |
| (0.4, 1.6, 2.0) | 7.32 | 4.10                 | 51.8         | 51.0                 | 47.4         | 46.6                 | 107          | 107  | 7.54 | 3.31   |
| (0.4, 1.8, 1.8) | 7.54 | 4.14                 | 54.6         | 53.5                 | 49.3         | 48.9                 | 104          | 104  | 7.58 | 3.30   |
| (0.4, 1.8, 2.0) | 6.65 | 3.90                 | 42.6         | 41.7                 | 40.8         | 40.0                 | 82.6         | 82.8 | 6.97 | 3.09   |
| (0.4, 2.0, 2.0) | 5.92 | 3.67                 | 33.5         | 32.4                 | 34.3         | 34.1                 | 65.1         | 64.2 | 6.39 | 2.87   |

Extended Table 8.2. (continued)

|                 |      |                      |      | p=3, | $\mu = 0$ |                      |     |                      |      |                      |
|-----------------|------|----------------------|------|------|-----------|----------------------|-----|----------------------|------|----------------------|
|                 | MCI  | $D_5(0)$             | S    | R    | S         | A                    | S   | V                    | LR   | $2C_5$               |
| λ               | ARL  | $\operatorname{SRL}$ | ARL  | SRL  | ARL       | $\operatorname{SRL}$ | ARL | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ |
| (0.6, 0.6, 0.6) | 16.7 | 5.17                 | 135  | 134  | 119       | 119                  | >1  | 952                  | 14.6 | 6.20                 |
| (0.6, 0.6, 0.8) | 18.7 | 6.58                 | 145  | 144  | 132       | 132                  | >18 | 849                  | 18.3 | 8.04                 |
| (0.6, 0.6, 1.0) | 19.1 | 7.11                 | 152  | 151  | 136       | 136                  | >1  | 644                  | 19.8 | 8.71                 |
| (0.6, 0.6, 1.2) | 19.2 | 7.31                 | 158  | 157  | 132       | 132                  | >13 | 379                  | 18.7 | 8.28                 |
| (0.6, 0.6, 1.4) | 18.2 | 7.58                 | 152  | 153  | 120       | 120                  | >1  | 094                  | 16.6 | 7.29                 |
| (0.6, 0.6, 1.6) | 16.1 | 7.72                 | 134  | 133  | 103       | 103                  | 840 | 656                  | 14.2 | 6.35                 |
| (0.6, 0.6, 1.8) | 13.4 | 7.23                 | 106  | 106  | 83.1      | 83.4                 | 629 | 554                  | 11.9 | 5.46                 |
| (0.6, 0.6, 2.0) | 11.1 | 6.75                 | 78.4 | 77.5 | 65.1      | 64.8                 | 476 | 447                  | 10.2 | 4.76                 |
| (0.6, 0.8, 0.8) | 22.0 | 9.20                 | 161  | 160  | 149       | 149                  | >1  | 559                  | 25.0 | 11.4                 |
| (0.6, 0.8, 1.0) | 23.0 | 10.1                 | 166  | 163  | 155       | 155                  | >1  | 184                  | 28.1 | 12.9                 |
| (0.6, 0.8, 1.2) | 22.7 | 10.3                 | 173  | 171  | 152       | 152                  | 839 | 660                  | 26.0 | 12.0                 |
| (0.6, 0.8, 1.4) | 20.8 | 10.2                 | 161  | 160  | 137       | 137                  | 572 | 517                  | 21.7 | 10.1                 |
| (0.6, 0.8, 1.6) | 17.8 | 9.74                 | 142  | 141  | 116       | 117                  | 398 | 384                  | 17.5 | 8.27                 |
| (0.6, 0.8, 1.8) | 14.3 | 8.67                 | 109  | 108  | 93.3      | 94.6                 | 293 | 288                  | 14.4 | 6.93                 |
| (0.6, 0.8, 2.0) | 11.4 | 7.52                 | 77.0 | 75.7 | 72.8      | 72.2                 | 220 | 220                  | 11.8 | 5.80                 |
| (0.6, 1.0, 1.0) | 23.8 | 11.1                 | 179  | 177  | 161       | 160                  | 763 | 625                  | 31.4 | 14.9                 |
| (0.6, 1.0, 1.2) | 23.1 | 11.4                 | 178  | 175  | 155       | 155                  | 473 | 450                  | 29.2 | 13.5                 |
| (0.6, 1.0, 1.4) | 21.0 | 10.9                 | 170  | 169  | 143       | 143                  | 311 | 307                  | 23.8 | 11.2                 |
| (0.6, 1.0, 1.6) | 17.7 | 10.2                 | 140  | 140  | 120       | 120                  | 216 | 212                  | 18.9 | 9.01                 |
| (0.6, 1.0, 1.8) | 14.0 | 8.80                 | 107  | 106  | 96.7      | 95.7                 | 163 | 163                  | 15.1 | 7.36                 |
| (0.6, 1.0, 2.0) | 11.1 | 7.64                 | 74.4 | 72.6 | 74.8      | 73.9                 | 126 | 125                  | 12.5 | 6.18                 |
| (0.6, 1.2, 1.2) | 22.2 | 11.4                 | 177  | 175  | 153       | 153                  | 293 | 288                  | 26.9 | 12.4                 |
| (0.6, 1.2, 1.4) | 20.0 | 10.9                 | 166  | 165  | 137       | 139                  | 193 | 192                  | 22.0 | 10.4                 |
| (0.6, 1.2, 1.6) | 16.7 | 9.86                 | 134  | 134  | 116       | 116                  | 138 | 137                  | 17.8 | 8.50                 |
| (0.6, 1.2, 1.8) | 13.2 | 8.54                 | 99.5 | 98.3 | 93.6      | 93.0                 | 104 | 104                  | 14.5 | 7.03                 |

 ${\bf Extended\ Table\ 8.2.\ (continued)}$ 

|                 |      |                      |      | p=3, | $\mu = 0$ |                      |      |                      |      |        |
|-----------------|------|----------------------|------|------|-----------|----------------------|------|----------------------|------|--------|
|                 | MCI  | $D_5(0)$             | S    | R    | S         | A                    | S    | V                    | LR   | $2C_5$ |
| λ               | ARL  | $\operatorname{SRL}$ | ARL  | SRL  | ARL       | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ | ARL  | SRL    |
| (0.6, 1.2, 2.0) | 10.5 | 7.23                 | 69.2 | 68.1 | 72.9      | 72.0                 | 82.6 | 82.8                 | 12.1 | 5.97   |
| (0.6, 1.4, 1.4) | 17.7 | 10.4                 | 149  | 149  | 125       | 125                  | 132  | 131                  | 19.0 | 8.88   |
| (0.6, 1.4, 1.6) | 14.8 | 9.28                 | 120  | 120  | 106       | 106                  | 96.3 | 96.6                 | 15.8 | 7.51   |
| (0.6, 1.4, 1.8) | 11.8 | 8.19                 | 87.2 | 86.3 | 85.8      | 85.6                 | 74.0 | 73.8                 | 13.3 | 6.43   |
| (0.6, 1.4, 2.0) | 9.47 | 6.89                 | 62.6 | 61.3 | 67.0      | 66.2                 | 59.0 | 58.8                 | 11.2 | 5.47   |
| (0.6, 1.6, 1.6) | 12.5 | 8.53                 | 95.6 | 95.1 | 91.2      | 91.0                 | 71.6 | 71.5                 | 13.6 | 6.47   |
| (0.6, 1.6, 1.8) | 10.2 | 7.37                 | 71.6 | 71.4 | 74.4      | 73.8                 | 55.7 | 54.4                 | 11.7 | 5.67   |
| (0.6, 1.6, 2.0) | 8.42 | 6.08                 | 53.3 | 52.5 | 58.9      | 58.1                 | 45.4 | 45.1                 | 10.0 | 4.82   |
| (0.6, 1.8, 1.8) | 8.70 | 6.26                 | 56.3 | 55.7 | 61.8      | 61.1                 | 44.1 | 44.0                 | 10.2 | 4.87   |
| (0.6, 1.8, 2.0) | 7.29 | 5.29                 | 43.1 | 42.2 | 50.2      | 49.3                 | 36.2 | 35.9                 | 9.02 | 4.38   |
| (0.6, 2.0, 2.0) | 6.21 | 4.52                 | 34.0 | 33.5 | 41.7      | 40.9                 | 29.7 | 28.7                 | 8.00 | 3.91   |
| (0.8, 0.8, 0.8) | 49.6 | 34.9                 | 177  | 175  | 177       | 182                  | >1   | 065                  | 47.6 | 25.4   |
| (0.8, 0.8, 1.0) | 61.2 | 46.1                 | 188  | 183  | 184       | 187                  | 649  | 566                  | 59.3 | 33.5   |
| (0.8, 0.8, 1.2) | 57.3 | 43.8                 | 191  | 187  | 173       | 173                  | 398  | 384                  | 50.1 | 27.3   |
| (0.8, 0.8, 1.4) | 43.4 | 34.6                 | 183  | 179  | 156       | 157                  | 265  | 262                  | 35.8 | 19.1   |
| (0.8, 0.8, 1.6) | 28.7 | 23.1                 | 150  | 150  | 132       | 134                  | 183  | 182                  | 25.5 | 13.4   |
| (0.8, 0.8, 1.8) | 18.8 | 15.7                 | 150  | 150  | 107       | 108                  | 138  | 137                  | 19.0 | 9.85   |
| (0.8, 0.8, 2.0) | 12.9 | 10.9                 | 78.1 | 76.3 | 82.7      | 82.0                 | 107  | 107                  | 15.0 | 7.89   |
| (0.8, 1.0, 1.0) | 78.0 | 64.0                 | 199  | 193  | 188       | 187                  | 356  | 346                  | 79.1 | 47.4   |
| (0.8, 1.0, 1.2) | 67.0 | 55.8                 | 200  | 195  | 185       | 187                  | 220  | 220                  | 63.7 | 36.7   |
| (0.8, 1.0, 1.4) | 45.6 | 39.0                 | 189  | 184  | 165       | 167                  | 147  | 147                  | 42.1 | 23.2   |
| (0.8, 1.0, 1.6) | 28.1 | 23.8                 | 154  | 152  | 139       | 140                  | 108  | 107                  | 28.4 | 15.2   |
| (0.8, 1.0, 1.8) | 17.9 | 15.1                 | 110  | 109  | 110       | 111                  | 82.4 | 82.3                 | 20.6 | 11.2   |
| (0.8, 1.0, 2.0) | 12.3 | 10.1                 | 75.0 | 73.3 | 85.5      | 84.4                 | 65.1 | 64.2                 | 15.7 | 8.37   |
| (0.8, 1.2, 1.2) | 57.2 | 49.5                 | 203  | 197  | 176       | 176                  | 139  | 137                  | 53.4 | 29.8   |

Extended Table 8.2. (continued)

|                 |      |                      |              | p=3,                 | $\mu = 0$    |                      |      |      |      |                      |
|-----------------|------|----------------------|--------------|----------------------|--------------|----------------------|------|------|------|----------------------|
|                 | MCI  | $D_5(0)$             | $\mathbf{S}$ | R                    | $\mathbf{S}$ | A                    | S    | V    | LF   | $C_5$                |
| λ               | ARL  | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL  | SRL  | ARL  | $\operatorname{SRL}$ |
| (0.8, 1.2, 1.4) | 38.5 | 33.4                 | 179          | 176                  | 160          | 162                  | 96.3 | 96.6 | 37.5 | 20.2                 |
| (0.8, 1.2, 1.6) | 24.4 | 21.6                 | 144          | 142                  | 133          | 134                  | 71.6 | 71.5 | 26.2 | 14.0                 |
| (0.8, 1.2, 1.8) | 16.1 | 13.9                 | 102          | 101                  | 107          | 108                  | 55.7 | 54.4 | 19.3 | 10.2                 |
| (0.8, 1.2, 2.0) | 11.3 | 9.75                 | 69.9         | 68.6                 | 82.9         | 81.6                 | 45.4 | 45.1 | 15.0 | 7.99                 |
| (0.8, 1.4, 1.4) | 28.0 | 24.7                 | 157          | 156                  | 145          | 147                  | 68.7 | 68.4 | 29.0 | 15.3                 |
| (0.8, 1.4, 1.6) | 19.3 | 16.3                 | 124          | 122                  | 122          | 124                  | 51.7 | 50.6 | 21.8 | 11.4                 |
| (0.8, 1.4, 1.8) | 13.5 | 11.8                 | 88.3         | 87.7                 | 98.1         | 98.1                 | 41.2 | 41.2 | 17.1 | 8.90                 |
| (0.8, 1.4, 2.0) | 9.91 | 8.41                 | 61.7         | 60.1                 | 76.2         | 75.8                 | 33.5 | 32.8 | 13.5 | 7.02                 |
| (0.8, 1.6, 1.6) | 14.7 | 12.9                 | 97.3         | 95.7                 | 104          | 106                  | 39.7 | 38.9 | 17.7 | 9.07                 |
| (0.8, 1.6, 1.8) | 11.0 | 9.16                 | 71.4         | 72.1                 | 85.2         | 85.0                 | 31.9 | 30.9 | 14.5 | 7.37                 |
| (0.8, 1.6, 2.0) | 8.67 | 7.10                 | 51.7         | 51.0                 | 67.7         | 67.6                 | 26.6 | 25.6 | 12.1 | 6.28                 |
| (0.8, 1.8, 1.8) | 8.90 | 7.54                 | 55.5         | 55.5                 | 70.9         | 70.8                 | 26.2 | 25.8 | 12.2 | 6.23                 |
| (0.8, 1.8, 2.0) | 7.33 | 5.88                 | 42.1         | 41.5                 | 56.6         | 55.7                 | 22.1 | 21.7 | 10.5 | 5.41                 |
| (0.8, 2.0, 2.0) | 6.17 | 4.81                 | 32.8         | 31.9                 | 46.7         | 46.2                 | 22.1 | 21.7 | 9.20 | 4.76                 |
| (1.0, 1.0, 1.0) | 207  | 195                  | 213          | 205                  | 205          | 208                  | 197  | 196  | 200  | 188                  |
| (1.0, 1.0, 1.2) | 122  | 117                  | 212          | 205                  | 198          | 199                  | 125  | 125  | 127  | 93.8                 |
| (1.0, 1.0, 1.4) | 58.6 | 55.6                 | 197          | 191                  | 174          | 175                  | 87.6 | 87.1 | 62.4 | 38.0                 |
| (1.0, 1.0, 1.6) | 30.0 | 27.5                 | 151          | 150                  | 149          | 149                  | 65.6 | 65.2 | 35.8 | 20.6                 |
| (1.0, 1.0, 1.8) | 17.8 | 16.2                 | 108          | 108                  | 118          | 117                  | 51.3 | 50.2 | 24.0 | 13.4                 |
| (1.0, 1.0, 2.0) | 12.1 | 10.7                 | 72.8         | 71.4                 | 90.7         | 90.5                 | 41.8 | 41.7 | 17.7 | 9.93                 |
| (1.0, 1.2, 1.2) | 78.5 | 76.2                 | 213          | 206                  | 190          | 192                  | 82.6 | 82.8 | 90.7 | 59.0                 |
| (1.0, 1.2, 1.4) | 43.2 | 41.5                 | 187          | 182                  | 171          | 172                  | 59.0 | 58.0 | 52.3 | 30.6                 |
| (1.0, 1.2, 1.6) | 24.9 | 22.5                 | 143          | 141                  | 144          | 144                  | 45.4 | 45.1 | 32.5 | 18.2                 |
| (1.0, 1.2, 1.8) | 15.8 | 14.0                 | 98.9         | 97.4                 | 114          | 114                  | 36.2 | 35.9 | 22.7 | 12.7                 |
| (1.0, 1.2, 2.0) | 10.9 | 9.60                 | 66.9         | 65.8                 | 87.4         | 87.0                 | 29.7 | 28.7 | 16.8 | 9.13                 |

Extended Table 8.2. (continued)

|                 |      |                      |      | p=3, | $\mu = 0$ |                      |      |                      |      |        |
|-----------------|------|----------------------|------|------|-----------|----------------------|------|----------------------|------|--------|
|                 | MCI  | $D_5(0)$             | S    | R    | S         | A                    | S    | V                    | LR   | $2C_5$ |
| λ               | ARL  | $\operatorname{SRL}$ | ARL  | SRL  | ARL       | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ | ARL  | SRL    |
| (1.0, 1.4, 1.4) | 28.5 | 27.0                 | 157  | 157  | 153       | 154                  | 43.4 | 43.4                 | 36.8 | 20.6   |
| (1.0, 1.4, 1.6) | 19.0 | 17.6                 | 121  | 121  | 130       | 132                  | 33.5 | 32.8                 | 26.2 | 14.3   |
| (1.0, 1.4, 1.8) | 13.1 | 11.6                 | 85.5 | 84.5 | 104       | 105                  | 27.4 | 26.1                 | 19.3 | 10.3   |
| (1.0, 1.4, 2.0) | 9.58 | 8.23                 | 59.3 | 58.2 | 80.9      | 81.2                 | 23.1 | 22.8                 | 15.0 | 8.02   |
| (1.0, 1.6, 1.6) | 14.1 | 12.6                 | 94.4 | 94.0 | 111       | 112                  | 26.7 | 26.3                 | 20.2 | 10.8   |
| (1.0, 1.6, 1.8) | 10.5 | 9.26                 | 68.4 | 68.5 | 90.0      | 89.6                 | 22.0 | 21.1                 | 16.0 | 8.49   |
| (1.0, 1.6, 2.0) | 8.29 | 6.88                 | 49.1 | 48.7 | 70.4      | 69.9                 | 18.6 | 18.1                 | 13.1 | 7.02   |
| (1.0, 1.8, 1.8) | 8.68 | 7.22                 | 53.5 | 52.1 | 74.7      | 74.0                 | 18.2 | 17.6                 | 13.4 | 7.10   |
| (1.0, 1.8, 2.0) | 7.03 | 5.65                 | 40.1 | 39.6 | 59.5      | 58.5                 | 15.7 | 15.1                 | 11.2 | 5.84   |
| (1.0, 2.0, 2.0) | 5.97 | 4.63                 | 31.2 | 30.3 | 49.6      | 49.6                 | 13.4 | 12.7                 | 9.71 | 5.06   |
| (1.2, 1.2, 1.2) | 60.6 | 60.4                 | 208  | 202  | 191       | 193                  | 55.9 | 55.8                 | 95.6 | 62.8   |
| (1.2, 1.2, 1.4) | 35.6 | 33.9                 | 175  | 173  | 169       | 171                  | 41.1 | 40.1                 | 53.7 | 31.6   |
| (1.2, 1.2, 1.6) | 21.7 | 19.9                 | 133  | 133  | 143       | 143                  | 32.3 | 31.9                 | 33.1 | 18.6   |
| (1.2, 1.2, 1.8) | 14.3 | 12.8                 | 92.4 | 90.9 | 114       | 114                  | 26.1 | 25.8                 | 22.8 | 12.5   |
| (1.2, 1.2, 2.0) | 10.3 | 8.88                 | 62.9 | 62.1 | 87.9      | 87.7                 | 22.1 | 21.7                 | 16.9 | 9.25   |
| (1.2, 1.4, 1.4) | 24.3 | 22.6                 | 148  | 148  | 153       | 154                  | 30.9 | 29.9                 | 37.6 | 21.1   |
| (1.2, 1.4, 1.6) | 16.9 | 15.4                 | 113  | 112  | 129       | 130                  | 24.6 | 24.2                 | 26.5 | 14.5   |
| (1.2, 1.4, 1.8) | 12.0 | 10.6                 | 78.9 | 77.7 | 104       | 104                  | 20.3 | 19.4                 | 19.5 | 10.4   |
| (1.2, 1.4, 2.0) | 9.08 | 7.77                 | 55.1 | 54.0 | 80.4      | 79.2                 | 17.3 | 16.5                 | 15.2 | 8.26   |
| (1.2, 1.6, 1.6) | 12.7 | 11.3                 | 86.9 | 87.1 | 111       | 112                  | 19.8 | 19.3                 | 20.6 | 11.1   |
| (1.2, 1.6, 1.8) | 9.81 | 8.40                 | 64.1 | 63.3 | 89.9      | 89.7                 | 16.5 | 15.9                 | 16.2 | 8.53   |
| (1.2, 1.6, 2.0) | 7.74 | 6.38                 | 45.9 | 45.3 | 71.0      | 69.9                 | 14.2 | 13.6                 | 13.2 | 7.00   |
| (1.2, 1.8, 1.8) | 8.05 | 6.73                 | 49.6 | 45.3 | 74.8      | 74.3                 | 14.1 | 13.5                 | 13.4 | 7.02   |
| (1.2, 1.8, 2.0) | 6.60 | 5.39                 | 37.2 | 36.5 | 59.6      | 59.0                 | 12.3 | 11.8                 | 11.4 | 5.97   |
| (1.2, 2.0, 2.0) | 5.67 | 4.37                 | 29.3 | 29.1 | 48.9      | 48.3                 | 10.5 | 10.0                 | 9.85 | 5.17   |

Extended Table 8.2. (continued)

|                 |      |                      |      | p=3,                 | $\mu = 0$ |                      |              |                      |      |                      |
|-----------------|------|----------------------|------|----------------------|-----------|----------------------|--------------|----------------------|------|----------------------|
|                 | MCI  | $D_5(0)$             | S    | R                    | S         | A                    | $\mathbf{S}$ | V                    | LR   | $2C_5$               |
| λ               | ARL  | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ | ARL       | $\operatorname{SRL}$ | ARL          | $\operatorname{SRL}$ | ARL  | $\operatorname{SRL}$ |
| (1.4, 1.4, 1.4) | 19.7 | 18.3                 | 130  | 128                  | 144       | 144                  | 23.8         | 23.5                 | 32.4 | 17.7                 |
| (1.4, 1.4, 1.6) | 14.4 | 12.9                 | 97.8 | 98.9                 | 122       | 121                  | 19.3         | 18.5                 | 23.9 | 12.8                 |
| (1.4, 1.4, 1.8) | 10.5 | 9.18                 | 69.6 | 69.8                 | 99.1      | 99.2                 | 16.1         | 15.5                 | 18.2 | 9.75                 |
| (1.4, 1.4, 2.0) | 8.15 | 6.82                 | 49.1 | 48.3                 | 76.9      | 76.4                 | 13.8         | 13.2                 | 14.3 | 7.73                 |
| (1.4, 1.6, 1.6) | 11.1 | 9.82                 | 76.3 | 75.7                 | 105       | 105                  | 15.8         | 15.2                 | 18.9 | 10.0                 |
| (1.4, 1.6, 1.8) | 8.79 | 7.45                 | 56.3 | 56.3                 | 85.6      | 85.3                 | 13.4         | 12.9                 | 15.2 | 7.99                 |
| (1.4, 1.6, 2.0) | 7.13 | 5.90                 | 41.7 | 40.8                 | 67.7      | 67.7                 | 11.5         | 10.9                 | 12.5 | 6.60                 |
| (1.4, 1.8, 1.8) | 7.39 | 6.08                 | 44.1 | 43.4                 | 71.0      | 70.3                 | 11.3         | 10.7                 | 12.8 | 6.72                 |
| (1.4, 1.8, 2.0) | 6.16 | 4.92                 | 33.7 | 33.0                 | 57.8      | 57.7                 | 9.90         | 9.43                 | 10.8 | 5.61                 |
| (1.4, 2.0, 2.0) | 5.36 | 4.07                 | 26.4 | 25.8                 | 47.0      | 46.8                 | 8.84         | 8.17                 | 9.42 | 4.86                 |
| (1.6, 1.6, 1.6) | 9.51 | 8.24                 | 63.2 | 62.6                 | 94.3      | 92.5                 | 13.1         | 12.6                 | 16.7 | 8.73                 |
| (1.6, 1.6, 1.8) | 7.78 | 6.42                 | 47.6 | 47.8                 | 77.8      | 77.4                 | 11.1         | 10.5                 | 13.8 | 7.19                 |
| (1.6, 1.6, 2.0) | 6.49 | 5.22                 | 36.2 | 35.5                 | 62.4      | 62.3                 | 9.73         | 9.30                 | 11.5 | 5.92                 |
| (1.6, 1.8, 1.8) | 6.60 | 5.25                 | 37.8 | 37.4                 | 64.9      | 64.4                 | 9.59         | 9.14                 | 11.7 | 6.07                 |
| (1.6, 1.8, 2.0) | 5.68 | 4.43                 | 29.6 | 28.9                 | 53.0      | 52.8                 | 8.46         | 7.96                 | 10.1 | 5.24                 |
| (1.6, 2.0, 2.0) | 4.96 | 3.72                 | 23.9 | 23.5                 | 44.0      | 43.8                 | 7.59         | 6.95                 | 8.92 | 4.59                 |
| (1.8, 1.8, 1.8) | 5.93 | 4.62                 | 32.2 | 31.4                 | 57.7      | 56.8                 | 8.44         | 7.83                 | 10.6 | 5.42                 |
| (1.8, 1.8, 2.0) | 5.16 | 3.95                 | 25.5 | 25.2                 | 47.1      | 47.0                 | 7.38         | 6.88                 | 9.29 | 4.75                 |
| (1.8, 2.0, 2.0) | 4.61 | 3.41                 | 21.1 | 20.8                 | 39.8      | 39.0                 | 6.54         | 6.04                 | 8.28 | 4.21                 |
| (2.0, 2.0, 2.0) | 4.23 | 3.10                 | 18.1 | 17.7                 | 35.2      | 34.7                 | 5.87         | 5.35                 | 7.60 | 3.88                 |

**Extended Table 9.1.** The out-of-control ARL and SRL of  $MCD_2(0)$  with p = 3,  $\mu = 0$ , h = 10/0.74,  $k_u = 1.5/0.74$ ,  $k_l = 0.5/0.74$  and the in-control (ARL,SRL)= (170, 161) where  $\lambda = \lambda(\Sigma_o^{-1/2}\Sigma\Sigma_o^{-1/2})$ .

| λ               | ARL  | SRL  | λ               | ARL  | SRL  | λ               | ARL  | SRL  |
|-----------------|------|------|-----------------|------|------|-----------------|------|------|
| (0.2, 0.2, 0.2) | 24.9 | 1.49 | (0.2, 0.8, 1.4) | 26.0 | 5.89 | (0.4, 0.4, 1.4) | 33.4 | 9.44 |
| (0.2, 0.2, 0.4) | 25.7 | 1.83 | (0.2, 0.8, 1.6) | 24.5 | 7.20 | (0.4, 0.4, 1.6) | 30.7 | 10.9 |
| (0.2, 0.2, 0.6) | 25.8 | 1.88 | (0.2, 0.8, 1.8) | 22.7 | 8.16 | (0.4, 0.4, 1.8) | 27.7 | 11.9 |
| (0.2, 0.2, 0.8) | 25.8 | 2.00 | (0.2, 0.8, 2.0) | 20.7 | 8.85 | (0.4, 0.4, 2.0) | 24.6 | 12.2 |
| (0.2, 0.2, 1.0) | 25.8 | 2.23 | (0.2, 1.0, 1.0) | 27.4 | 3.93 | (0.4, 0.6, 0.6) | 39.0 | 8.48 |
| (0.2, 0.2, 1.2) | 25.5 | 3.03 | (0.2, 1.0, 1.2) | 26.7 | 5.04 | (0.4, 0.6, 0.8) | 40.4 | 9.47 |
| (0.2, 0.2, 1.4) | 24.8 | 4.29 | (0.2, 1.0, 1.4) | 25.6 | 6.34 | (0.4, 0.6, 1.0) | 40.6 | 10.2 |
| (0.2, 0.2, 1.6) | 23.7 | 5.64 | (0.2, 1.0, 1.6) | 24.0 | 7.55 | (0.4, 0.6, 1.2) | 39.7 | 11.3 |
| (0.2, 0.2, 1.8) | 22.1 | 6.82 | (0.2, 1.0, 1.8) | 22.1 | 8.46 | (0.4, 0.6, 1.4) | 37.1 | 12.8 |
| (0.2, 0.2, 2.0) | 20.5 | 7.65 | (0.2, 1.0, 2.0) | 20.0 | 9.02 | (0.4, 0.6, 1.6) | 33.5 | 14.0 |
| (0.2, 0.4, 0.4) | 27.1 | 2.46 | (0.2, 1.2, 1.2) | 25.8 | 6.23 | (0.4, 0.6, 1.8) | 29.7 | 14.4 |
| (0.2, 0.4, 0.6) | 27.3 | 2.58 | (0.2, 1.2, 1.4) | 24.7 | 7.05 | (0.4, 0.6, 2.0) | 25.7 | 14.4 |
| (0.2, 0.4, 0.8) | 27.4 | 2.69 | (0.2, 1.2, 1.6) | 23.0 | 8.09 | (0.4, 0.8, 0.8) | 41.9 | 10.7 |
| (0.2, 0.4, 1.0) | 27.4 | 3.02 | (0.2, 1.2, 1.8) | 21.1 | 8.80 | (0.4, 0.8, 1.0) | 42.0 | 11.5 |
| (0.2, 0.4, 1.2) | 27.0 | 3.83 | (0.2, 1.2, 2.0) | 19.2 | 9.21 | (0.4, 0.8, 1.2) | 40.8 | 12.4 |
| (0.2, 0.4, 1.4) | 26.1 | 5.18 | (0.2, 1.4, 1.4) | 23.4 | 7.95 | (0.4, 0.8, 1.4) | 37.7 | 14.0 |
| (0.2, 0.4, 1.6) | 24.8 | 6.60 | (0.2, 1.4, 1.6) | 21.7 | 8.65 | (0.4, 0.8, 1.6) | 33.8 | 15.1 |
| (0.2, 0.4, 1.8) | 23.1 | 7.68 | (0.2, 1.4, 1.8) | 19.9 | 9.13 | (0.4, 0.8, 1.8) | 29.6 | 15.2 |
| (0.2, 0.4, 2.0) | 21.2 | 8.42 | (0.2, 1.4, 2.0) | 18.0 | 9.32 | (0.4, 0.8, 2.0) | 25.4 | 14.8 |
| (0.2, 0.6, 0.6) | 27.6 | 2.80 | (0.2, 1.6, 1.6) | 20.1 | 9.06 | (0.4, 1.0, 1.0) | 41.7 | 12.3 |
| (0.2, 0.6, 0.8) | 27.7 | 2.88 | (0.2, 1.6, 1.8) | 18.4 | 9.28 | (0.4, 1.0, 1.2) | 40.2 | 13.3 |
| (0.2, 0.6, 1.0) | 27.6 | 3.22 | (0.2, 1.6, 2.0) | 16.7 | 9.24 | (0.4, 1.0, 1.4) | 36.8 | 14.7 |
| (0.2, 0.6, 1.2) | 27.2 | 4.13 | (0.2, 1.8, 1.8) | 16.9 | 9.27 | (0.4, 1.0, 1.6) | 32.8 | 15.5 |
| (0.2, 0.6, 1.4) | 26.2 | 5.61 | (0.2, 1.8, 2.0) | 15.3 | 9.05 | (0.4, 1.0, 1.8) | 28.4 | 15.4 |
| (0.2, 0.6, 1.6) | 24.7 | 6.94 | (0.2, 2.0, 2.0) | 13.9 | 8.81 | (0.4, 1.0, 2.0) | 24.4 | 14.9 |
| (0.2, 0.6, 1.8) | 23.0 | 7.95 | (0.4, 0.4, 0.4) | 32.8 | 4.88 | (0.4, 1.2, 1.2) | 37.9 | 14.4 |
| (0.2, 0.6, 2.0) | 21.0 | 8.67 | (0.4, 0.4, 0.6) | 35.0 | 6.14 | (0.4, 1.2, 1.4) | 34.7 | 15.3 |
| (0.2, 0.8, 0.8) | 27.7 | 3.03 | (0.4, 0.4, 0.8) | 35.7 | 6.48 | (0.4, 1.2, 1.6) | 30.6 | 15.7 |
| (0.2, 0.8, 1.0) | 27.6 | 3.40 | (0.4, 0.4, 1.0) | 35.7 | 7.03 | (0.4, 1.2, 1.8) | 26.6 | 15.1 |
| (0.2, 0.8, 1.2) | 27.1 | 4.34 | (0.4, 0.4, 1.2) | 35.1 | 7.92 | (0.4, 1.2, 2.0) | 22.9 | 14.6 |

Extended Table 9.1. (continued)

| λ               | ARL  | SRL  | λ               | ARL  | SRL  | λ               | ARL  | SRL  |
|-----------------|------|------|-----------------|------|------|-----------------|------|------|
| (0.4, 1.4, 1.4) | 31.6 | 15.6 | (0.6, 1.2, 1.2) | 63.6 | 42.0 | (0.8, 1.2, 1.8) | 32.3 | 28.5 |
| (0.4, 1.4, 1.6) | 27.9 | 15.5 | (0.6, 1.2, 1.4) | 51.9 | 37.1 | (0.8, 1.2, 2.0) | 25.2 | 22.0 |
| (0.4, 1.4, 1.8) | 24.3 | 14.9 | (0.6, 1.2, 1.6) | 40.9 | 30.9 | (0.8, 1.4, 1.4) | 47.6 | 42.8 |
| (0.4, 1.4, 2.0) | 21.0 | 14.0 | (0.6, 1.2, 1.8) | 31.8 | 24.6 | (0.8, 1.4, 1.6) | 35.5 | 32.0 |
| (0.4, 1.6, 1.6) | 24.7 | 15.1 | (0.6, 1.2, 2.0) | 25.5 | 20.2 | (0.8, 1.4, 1.8) | 27.5 | 24.4 |
| (0.4, 1.6, 1.8) | 21.7 | 14.2 | (0.6, 1.4, 1.4) | 43.1 | 32.5 | (0.8, 1.4, 2.0) | 22.1 | 19.4 |
| (0.4, 1.6, 2.0) | 18.8 | 13.1 | (0.6, 1.4, 1.6) | 34.4 | 27.1 | (0.8, 1.6, 1.6) | 28.2 | 25.2 |
| (0.4, 1.8, 1.8) | 19.0 | 13.2 | (0.6, 1.4, 1.8) | 27.7 | 22.1 | (0.8, 1.6, 1.8) | 23.0 | 20.1 |
| (0.4, 1.8, 2.0) | 16.8 | 12.2 | (0.6, 1.4, 2.0) | 22.7 | 18.5 | (0.8, 1.6, 2.0) | 18.9 | 16.2 |
| (0.4, 2.0, 2.0) | 14.8 | 11.0 | (0.6, 1.6, 1.6) | 28.3 | 22.9 | (0.8, 1.8, 1.8) | 19.3 | 16.8 |
| (0.6, 0.6, 0.6) | 51.8 | 16.8 | (0.6, 1.6, 1.8) | 23.6 | 19.1 | (0.8, 1.8, 2.0) | 16.3 | 13.7 |
| (0.6, 0.6, 0.8) | 59.2 | 22.9 | (0.6, 1.6, 2.0) | 19.6 | 16.0 | (0.8, 2.0, 2.0) | 14.2 | 11.9 |
| (0.6, 0.6, 1.0) | 60.8 | 26.2 | (0.6, 1.8, 1.8) | 20.0 | 16.4 | (1.0, 1.0, 1.2) | 116  | 109  |
| (0.6, 0.6, 1.2) | 58.5 | 27.1 | (0.6, 1.8, 2.0) | 17.0 | 13.9 | (1.0, 1.0, 1.4) | 73.1 | 68.7 |
| (0.6, 0.6, 1.4) | 51.8 | 26.3 | (0.6, 2.0, 2.0) | 14.8 | 12.1 | (1.0, 1.0, 1.6) | 48.5 | 45.5 |
| (0.6, 0.6, 1.6) | 43.7 | 25.1 | (0.8, 0.8, 0.8) | 126  | 87.0 | (1.0, 1.0, 1.8) | 34.1 | 31.0 |
| (0.6, 0.6, 1.8) | 35.8 | 22.6 | (0.8, 0.8, 1.0) | 146  | 111  | (1.0, 1.0, 2.0) | 26.0 | 22.9 |
| (0.6, 0.6, 2.0) | 29.4 | 20.2 | (0.8, 0.8, 1.2) | 120  | 95.1 | (1.0, 1.2, 1.2) | 82.8 | 79.9 |
| (0.6, 0.8, 0.8) | 74.3 | 37.1 | (0.8, 0.8, 1.4) | 83.9 | 68.3 | (1.0, 1.2, 1.4) | 56.7 | 53.7 |
| (0.6, 0.8, 1.0) | 78.0 | 42.2 | (0.8.0.8, 1.6)  | 57.2 | 47.8 | (1.0, 1.2, 1.6) | 40.0 | 37.7 |
| (0.6, 0.8, 1.2) | 72.4 | 41.1 | (0.8, 0.8, 1.8) | 40.3 | 34.3 | (1.0, 1.2, 1.8) | 29.7 | 26.9 |
| (0.6, 0.8, 1.4) | 60.6 | 37.9 | (0.8, 0.8, 2.0) | 30.2 | 25.6 | (1.0, 1.2, 2.0) | 23.3 | 20.6 |
| (0.6, 0.8, 1.6) | 48.1 | 32.4 | (0.8, 1.0, 1.0) | 163  | 140  | (1.0, 1.4, 1.4) | 42.5 | 39.4 |
| (0.6, 0.8, 1.8) | 37.4 | 26.9 | (0.8, 1.0, 1.2) | 122  | 107  | (1.0, 1.4, 1.6) | 32.1 | 29.4 |
| (0.6, 0.8, 2.0) | 29.6 | 22.3 | (0.8, 1.0, 1.4) | 80.3 | 71.0 | (1.0, 1.4, 1.8) | 25.3 | 22.7 |
| (0.6, 1.0, 1.0) | 80.6 | 47.1 | (0.8, 1.0, 1.6) | 53.2 | 46.9 | (1.0, 1.4, 2.0) | 20.5 | 17.7 |
| (0.6, 1.0, 1.2) | 72.8 | 44.9 | (0.8, 1.0, 1.8) | 37.3 | 33.1 | (1.0, 1.6, 1.6) | 25.8 | 23.1 |
| (0.6, 1.0, 1.4) | 58.9 | 39.8 | (0.8, 1.0, 2.0) | 28.2 | 24.5 | (1.0, 1.6, 1.8) | 21.3 | 18.7 |
| (0.6, 1.0, 1.6) | 46.2 | 33.0 | (0.8, 1.2, 1.2) | 91.6 | 82.3 | (1.0, 1.6, 2.0) | 17.6 | 15.0 |
| (0.6, 1.0, 1.8) | 35.5 | 26.5 | (0.8, 1.2, 1.4) | 63.7 | 57.3 | (1.0, 1.8, 1.8) | 18.0 | 15.5 |
| (0.6, 1.0, 2.0) | 28.0 | 21.7 | (0.8, 1.2, 1.6) | 44.6 | 40.3 | (1.0, 1.8, 2.0) | 15.3 | 13.0 |

Extended Table 9.1. (continued)

| λ               | ARL  | SRL  | λ               | ARL  | SRL  | λ               | ARL  | SRL  |
|-----------------|------|------|-----------------|------|------|-----------------|------|------|
| (1.0, 2.0, 2.0) | 13.4 | 11.3 | (1.6, 1.6, 1.6) | 17.1 | 14.6 | (1.2, 1.2, 1.2) | 62.3 | 58.8 |
| (1.6, 1.6, 1.8) | 14.8 | 12.5 | (1.2, 1.2, 1.4) | 45.3 | 42.3 | (1.6, 1.6, 2.0) | 13.0 | 10.7 |
| (1.2, 1.2, 1.6) | 33.7 | 30.9 | (1.6, 1.8, 1.8) | 13.1 | 11.0 | (1.2, 1.2, 1.8) | 26.1 | 23.2 |
| (1.6, 1.8, 2.0) | 11.7 | 9.49 | (1.2, 1.2, 2.0) | 21.1 | 18.5 | (1.6, 2.0, 2.0) | 10.6 | 8.54 |
| (1.2, 1.4, 1.4) | 35.4 | 32.5 | (1.8, 1.8, 1.8) | 11.8 | 9.60 | (1.2, 1.4, 1.6) | 27.8 | 25.0 |
| (1.8, 1.8, 2.0) | 10.7 | 8.61 | (1.2, 1.4, 1.8) | 22.6 | 20.0 | (1.8, 2.0, 2.0) | 9.76 | 7.75 |
| (1.2, 1.4, 2.0) | 18.5 | 16.0 | (2.0, 2.0, 2.0) | 8.91 | 6.96 | (1.2, 1.6, 1.6) | 22.9 | 20.1 |
| (1.2, 1.6, 1.8) | 19.1 | 16.6 | (1.2, 1.6, 2.0) | 16.1 | 13.7 | (1.2, 1.8, 1.8) | 16.4 | 14.2 |
| (1.2, 1.8, 2.0) | 14.2 | 12.0 | (1.2, 2.0, 2.0) | 12.6 | 10.4 | (1.4, 1.4, 1.4) | 29.0 | 26.4 |
| (1.4, 1.4, 1.6) | 23.7 | 21.2 | (1.4, 1.4, 1.8) | 19.5 | 16.9 | (1.4, 1.4, 2.0) | 16.4 | 13.9 |
| (1.4, 1.6, 1.6) | 19.9 | 17.2 | (1.4, 1.6, 1.8) | 16.9 | 17.2 | (1.4, 1.6, 2.0) | 14.5 | 12.2 |
| (1.4, 1.8, 1.8) | 14.7 | 12.6 | (1.4, 1.8, 2.0) | 12.9 | 10.7 | (1.4, 2.0, 2.0) | 11.5 | 9.38 |